



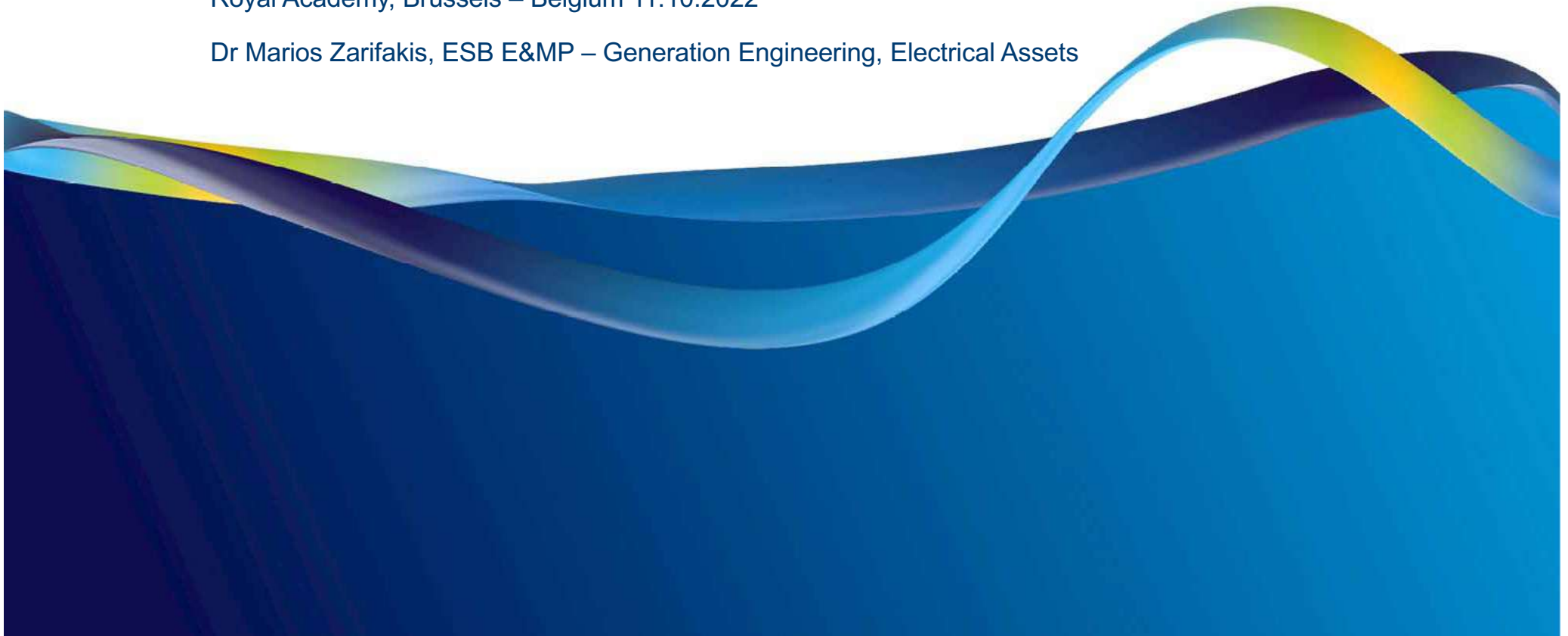
Energy for
generations

Challenges from increased Electricity Generation from Wind in Ireland

Meeting of the Energy Group of the European Physical Society

Royal Academy, Brussels – Belgium 11.10.2022

Dr Marios Zarifakis, ESB E&MP – Generation Engineering, Electrical Assets



Wind Mill and Wind Pump vs Wind Turbine



1. Driven to make a difference, Net Zero
2. A week in Ireland
3. Challenges
 - a) RoCoF - Rate of Change of Frequency: Increase of Frequency Volatility in Low Inertia Power Systems
 - Oscillations
 - Trips
4. Market Challenges in relation to “Delivering a Secure, Sustainable Electricity System” (DS3)
5. Synchronous Condensers and the Increase of Inertia in the System
6. SSR – Sub Synchronous Resonance: Damping of a synchronous condenser
7. Delivery through people
8. Commercial Challenges => Technical Challenges
9. Emerging Technologies

**DRIVEN TO MAKE
A DIFFERENCE**

NET ZERO
BY 2040

MAJOR EXTERNAL DEVELOPMENTS SINCE OUR PREVIOUS 2017 STRATEGY

Radical Shifts in Direction in Post-2017 Period



Accelerated Trends



AT ESB WE'RE DRIVEN TO MAKE A DIFFERENCE DELIVERING A BRIGHTER FUTURE



Creating and connecting sustainable, reliable affordable energy



Supporting the customers and communities we serve to achieve net zero



NET ZERO BY 2040

WE'VE ALWAYS BEEN DELIVERING A BRIGHTER FUTURE,
FOR THE CUSTOMERS AND COMMUNITIES WE SERVE



TODAY, THAT MEANS WE'RE DRIVEN TO MAKE A DIFFERENCE
- TO ACHIEVE NET ZERO BY 2040

DECARBONISED
ELECTRICITY

RESILIENT
INFRASTRUCTURE

EMPOWERED
CUSTOMERS

OUR PEOPLE • DIGITAL & DATA DRIVEN • FINANCIALLY STRONG • SUSTAINABLE & SOCIALLY RESPONSIBLE

OUR VALUES

WE'RE
COURAGEOUS

WE'RE
CARING

WE'RE
DRIVEN

WE'RE
TRUSTED

OUR ROLE

PURPOSE

At ESB, we're driven to make a difference.
 Delivering a brighter future; creating and connecting sustainable, reliable, affordable energy;
 and supporting the customers and communities we serve to achieve net zero.

WHAT WE WILL DO

DECARBONISED ELECTRICITY
 Develop and connect renewables to decarbonise the electricity system by 2040

RESILIENT INFRASTRUCTURE
 Provide resilient infrastructure for a reliable low carbon electricity system

EMPOWERED CUSTOMERS
 Empower, enable and support customers and communities to achieve net zero

FOUNDATIONAL CAPABILITIES

OUR PEOPLE
 Ensure we have the people capability to deliver our strategic objectives with a strong values-based and inclusive culture

DIGITAL & DATA DRIVEN
 Leveraging data and technology, transform ESB to a data driven digital utility

FINANCIALLY STRONG
 Maintain the financial performance and strength required to deliver our purpose

SUSTAINABLE & SOCIALLY RESPONSIBLE
 Step forward on social and environmental responsibility, cultivating a safe, sound and sustainable ethos in line with our values

HOW

OUR VALUES



THE SCALE OF OUR AMBITION

These are the most significant changes in strategic ambition from our previous 2017 strategy



Decarbonise ESB:
Science Based
Target 2030,
Net Zero 2040



Higher
renewable
targets



Faster, steeper
reduction in
carbon intensity



Increased focus on Island
of Ireland / GB investment
for specific purposes



Transform ESB
to a data driven
digital utility



Position for large
scale storage and
renewable balance



Transition
to reliable
low carbon
electricity system



Step forward on social and
environmental responsibility
- cultivating a safe, sound
and sustainable ethos
in line with our values



Scaled up ambition
for electrification of
heat and transport



Refocused
approach to
energy services



Ensure we have the people
capability to deliver our strategic
objectives, with a strong, values
based and inclusive culture

STRATEGIC AMBITION - ESB IN 2030 - KEY METRICS

	TODAY	2030
ESB renewable generation	976MW	> 5,000MW
Wind connected to networks (ROI + NI)	6.5GW	> 15GW
Share of ESB generation from zero carbon	~ 20%	63%
Networks asset base regulated (ROI + NI)	~ €11bn	> €16bn
EVs and heat pumps connected networks (ROI + NI)	~ 100k	~ 2m
Carbon intensity of generation fleet	414 gCO ₂ /kWh	<140 gCO ₂ /kWh
Home retrofits	Start up	35k
Satisfied customers	79-85%	> 85%
Premises passed with SIRO infrastructure	420k	770k

Strong alignment with Climate Action Plan

OUR VALUES

WE'RE
COURAGEOUS

Each of us is prepared to challenge the way we've always done things, stand up for what we feel is right and try better ways of working.

WE'RE
CARING

We're putting customers current and future needs at the heart of what we do and we keep ourselves and others safe and healthy.

WE'RE
DRIVEN

We bring passion and persistence to what we do everyday, innovating and collaborating to meet the challenges and opportunities ahead.

WE'RE
TRUSTED

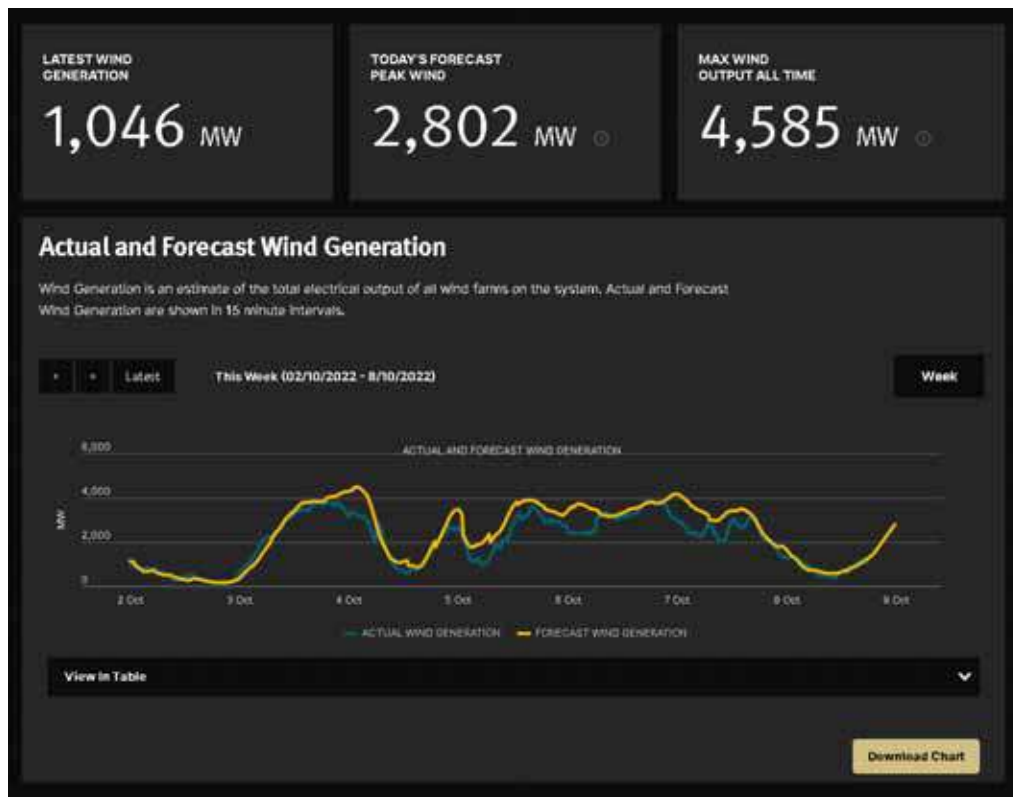
We each play our part, taking ownership of our responsibilities, seeing the job through and protecting our own health and safety, as well as others'.



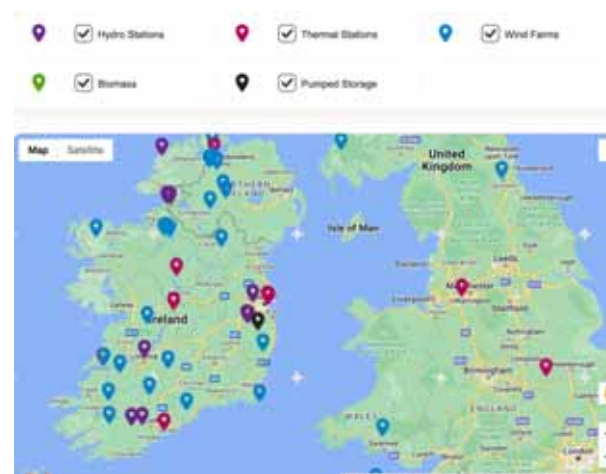
Wind Energy

At ESB, we want our wind farm investments to deliver long-term social, economic and environmental benefits for everyone. We believe in the power of wind energy and the potential it holds to change our world. As such, wind energy infrastructure is a core component of ESB's sustainability strategy.

A challenging Week - 2-8 October 2022



- High volatility in Wind Generation
- Challenging System Margins:
 - Some Units are out of service on planned overhauls
 - Demand on high availability and reliability of conventional generation capacity

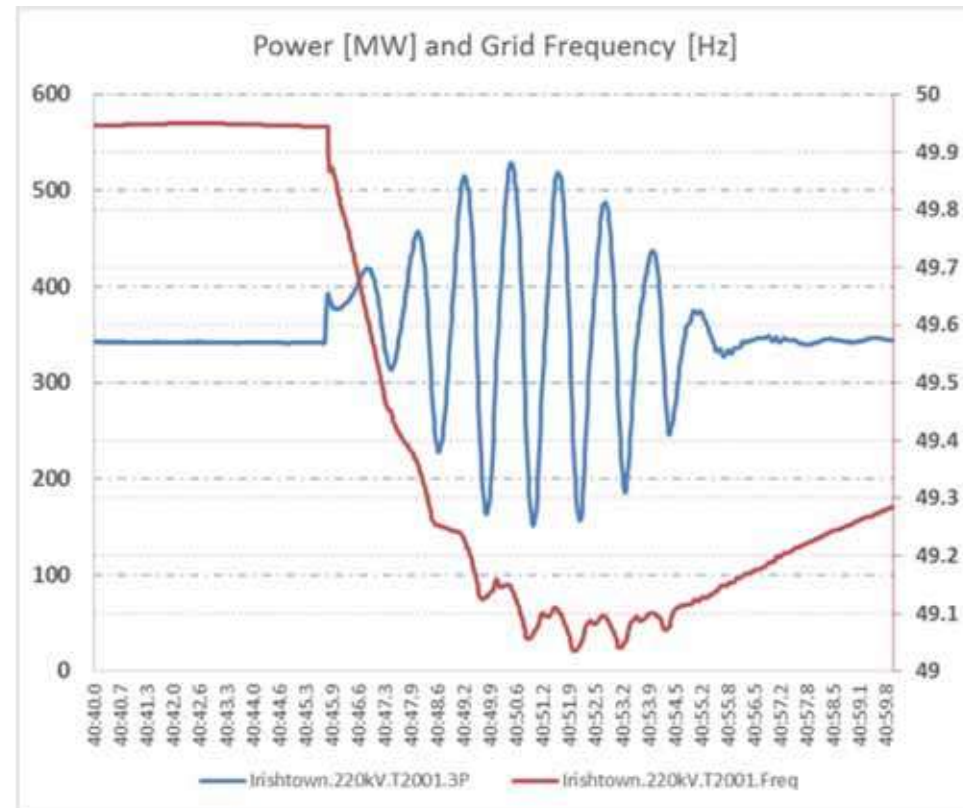


ESB Fleet

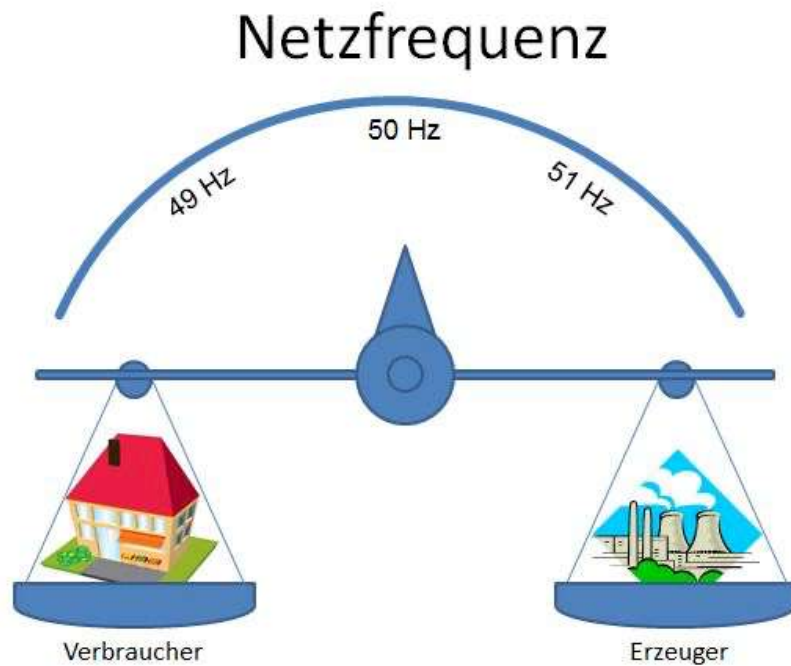
Real Event, Frequency Drop, DBP



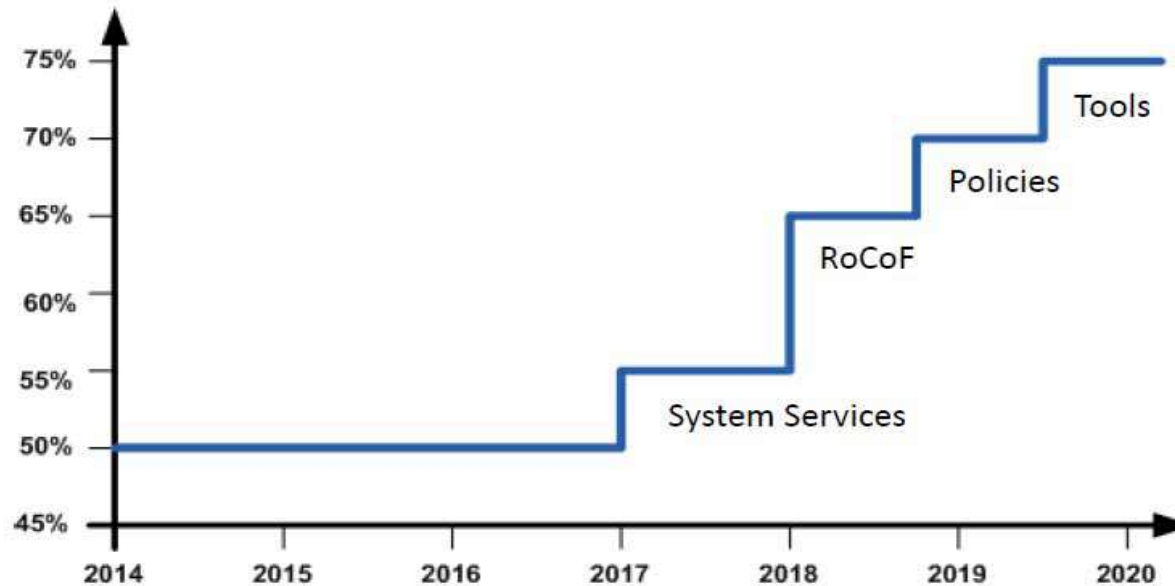
Fuel: Natural gas
Capacity: 410MW
Commissioned: 2002
Technology: Combined Cycle Gas Turbine (CCGT)



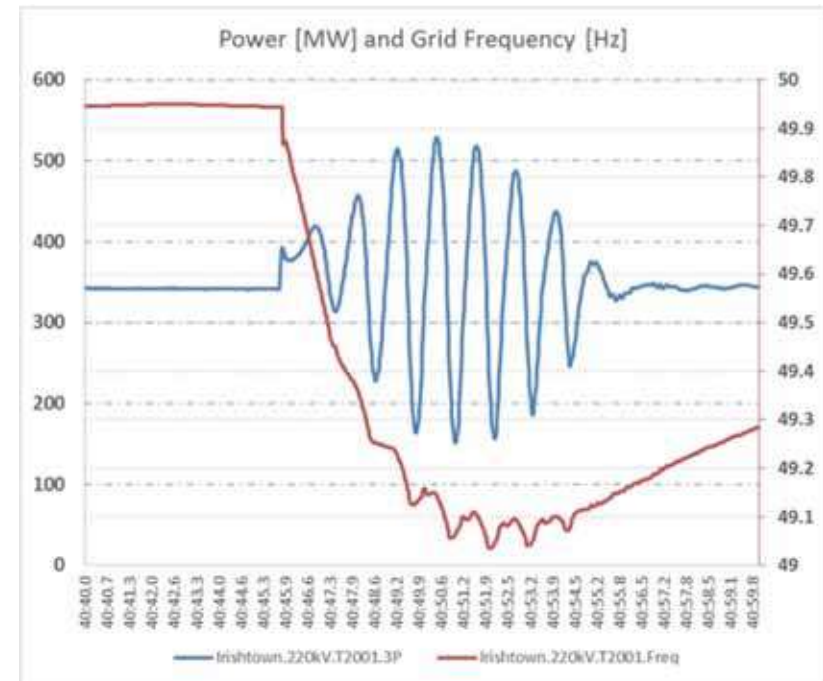
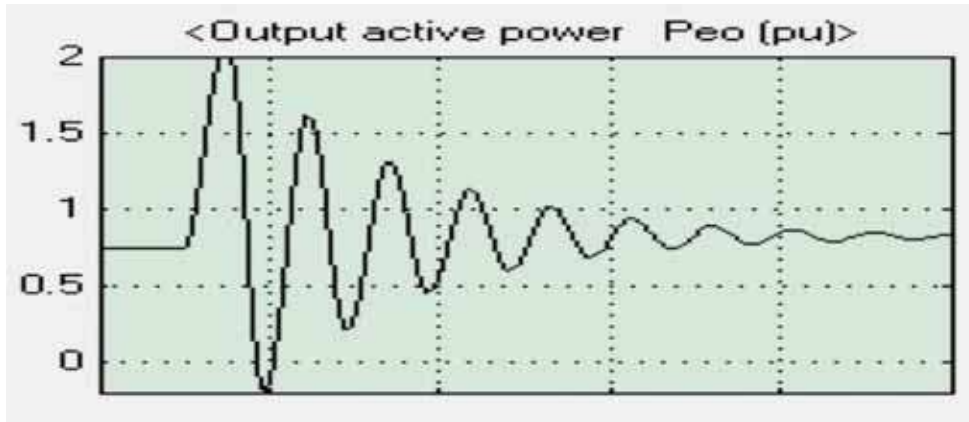
Electricity System Analogy



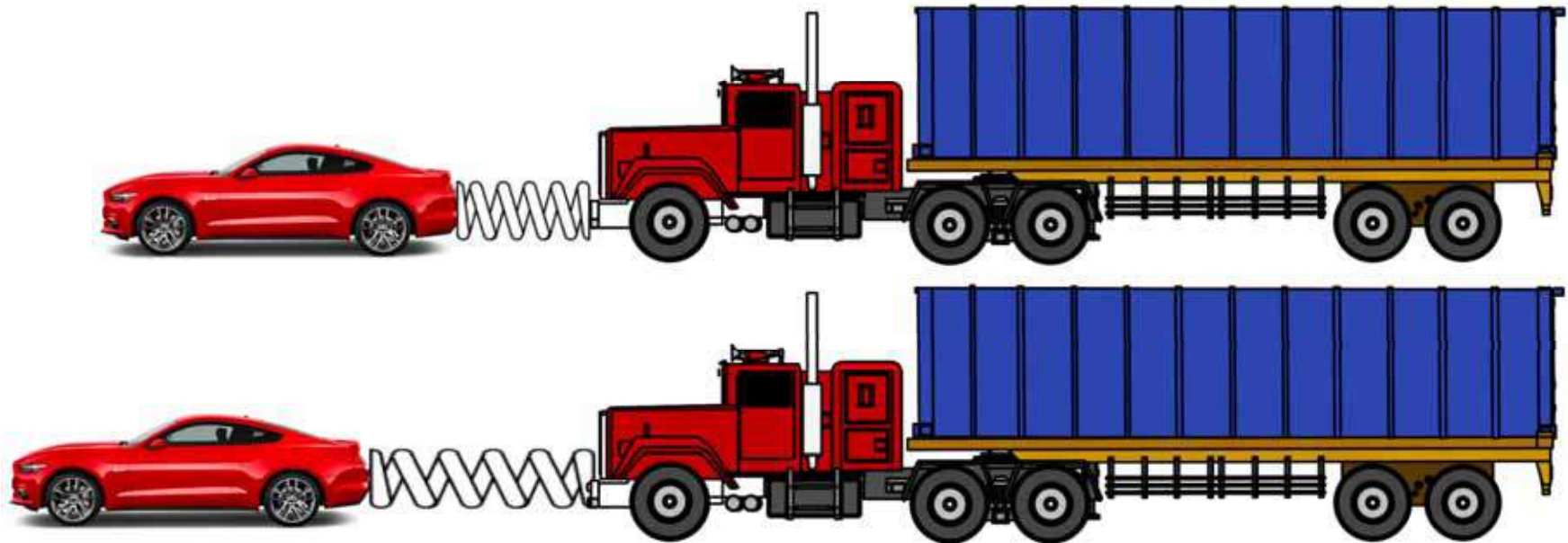
Operational Capability Outlook



“Continental Model” – Infinite Inertia vs “Island Model” – Finite Inertia



Car floors the Gas Pedal



Truck and Car drive at 100km/h, constant

Distance between Car and Truck indicates the power of car (how strong you push the gas)

Motorway analogy

All fine

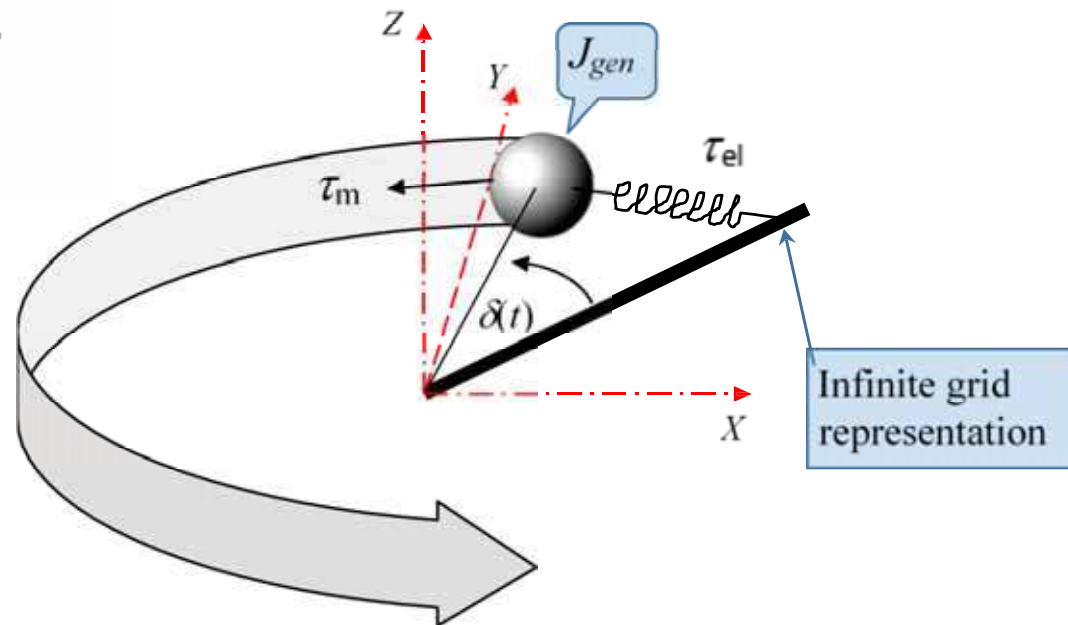
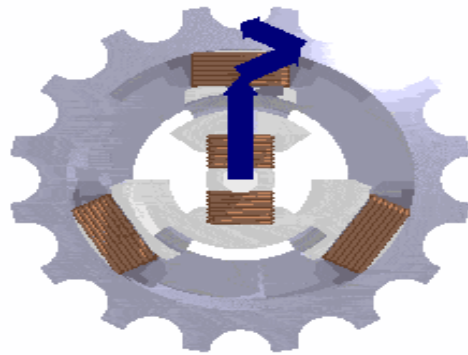


One truck cylinder gone

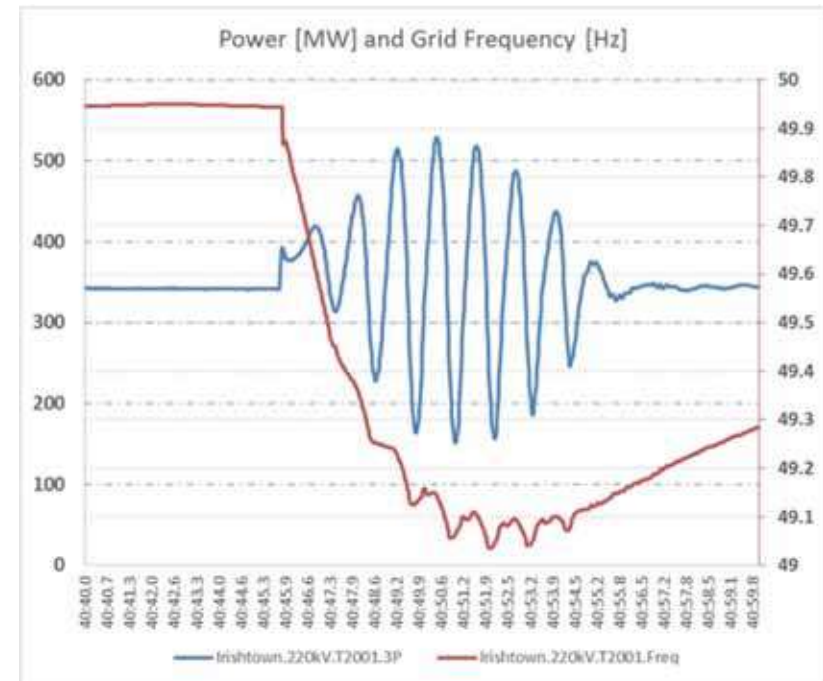
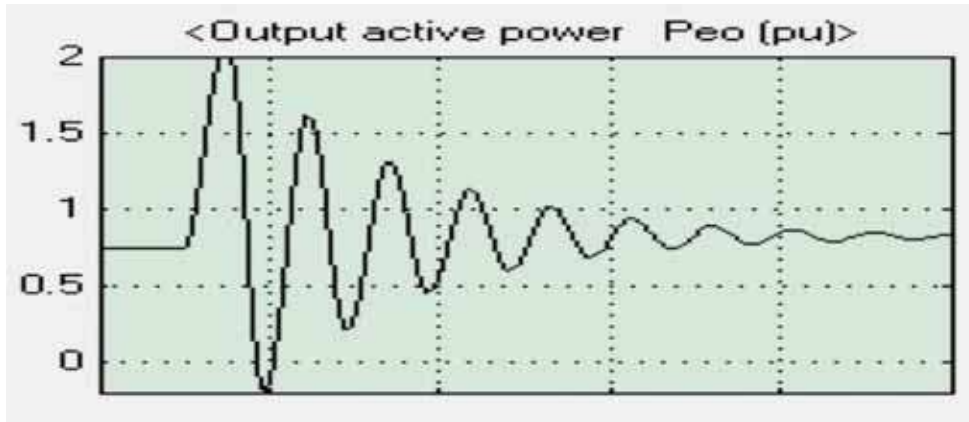


Stable with one cylinder less

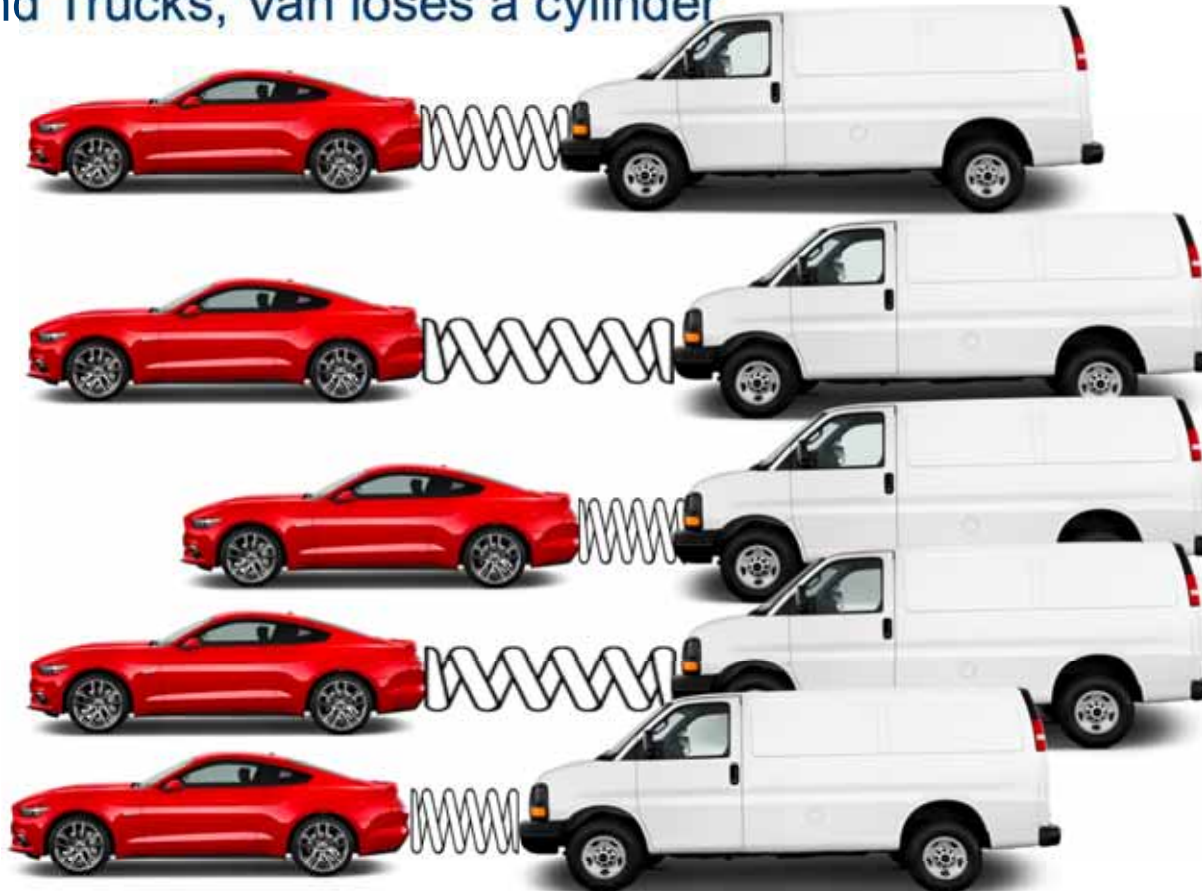




“Continental Model” – Infinite Inertia



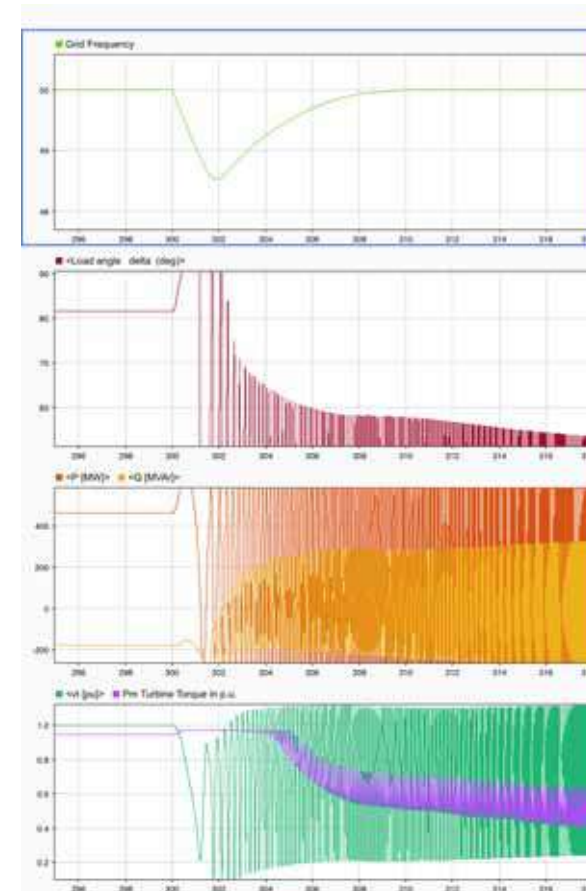
Cars and Trucks, Van loses a cylinder



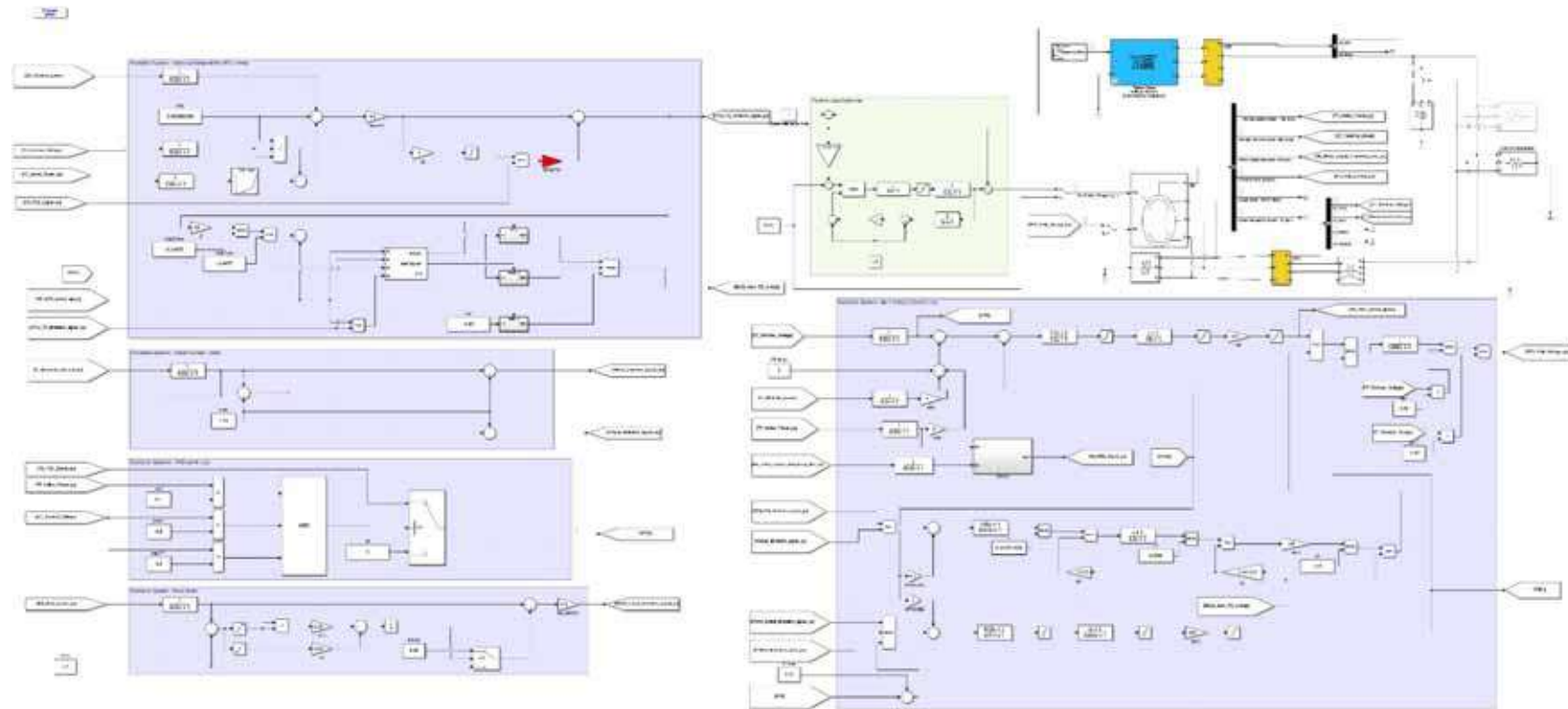
Trip due to Generator Pole Slip, Simulation after MXL2



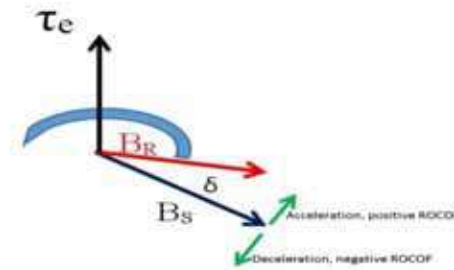
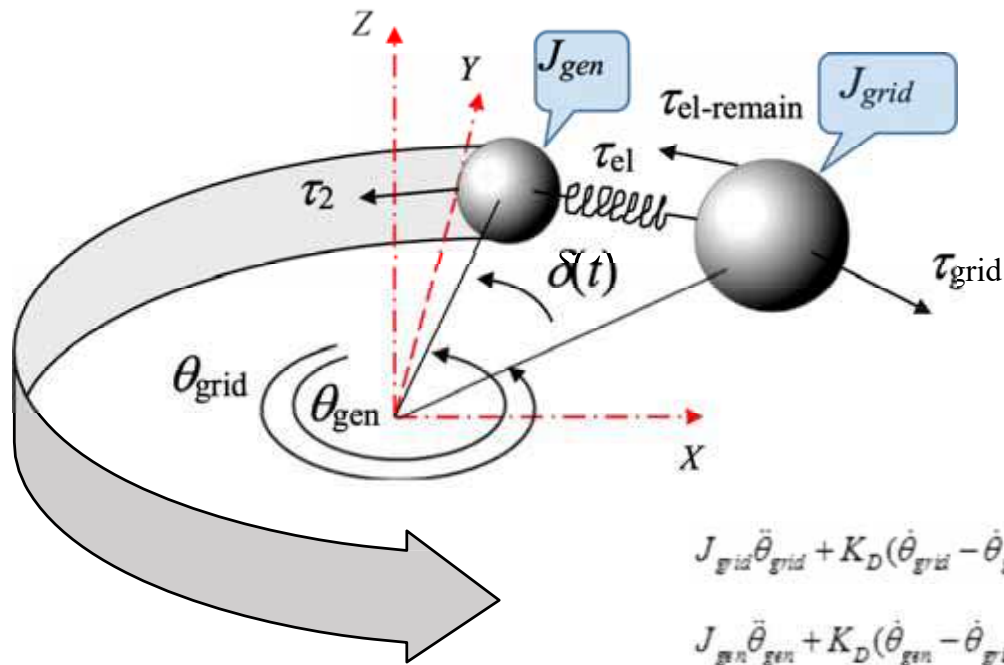
Aghada Unit 2, Single shaft CCGT
461 MW at generator terminals, 2010



Modelled Turbine Governor and Voltage Controller



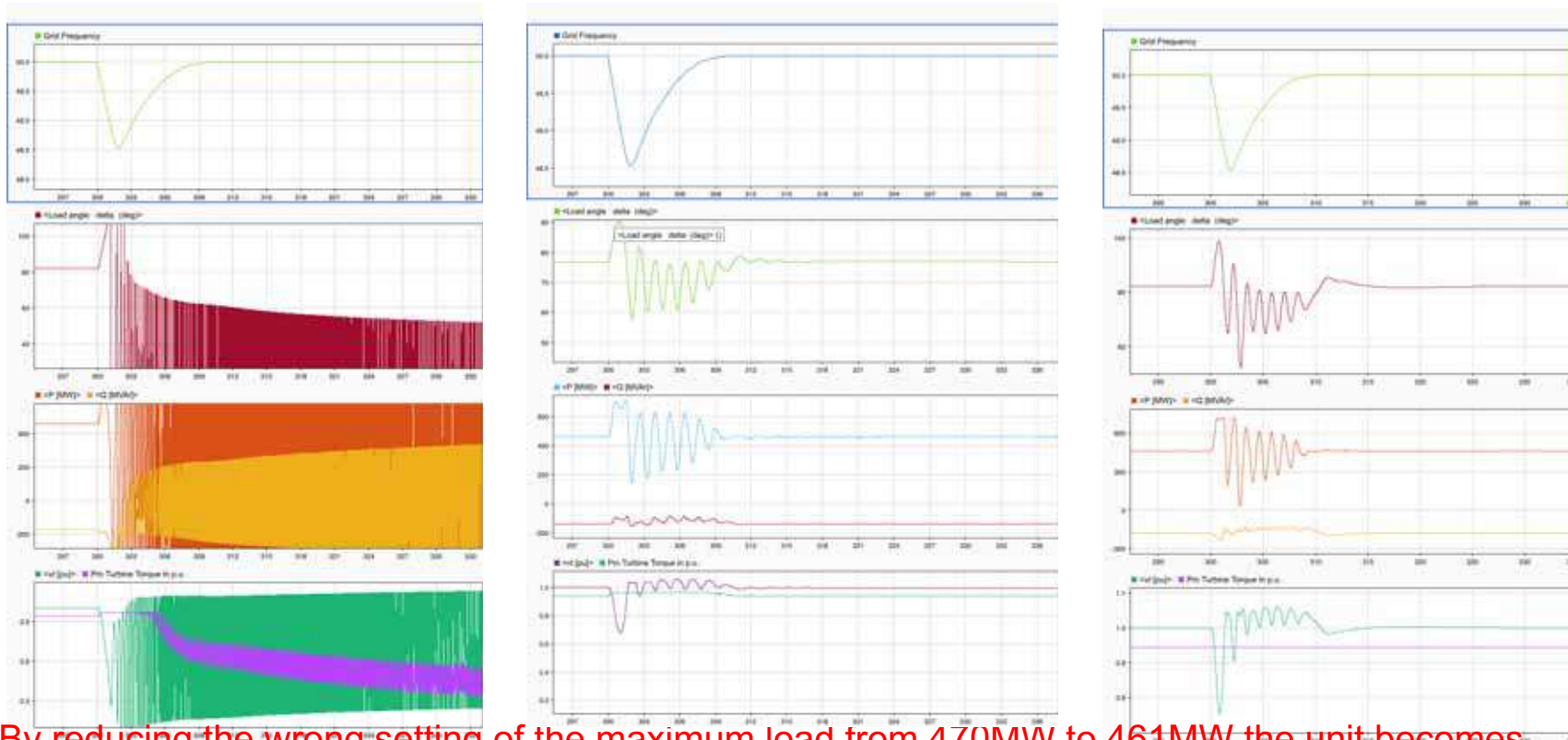
Equations of motion



$$J_{grid} \ddot{\theta}_{grid} + K_D (\dot{\theta}_{grid} - \dot{\theta}_{gen}) + \tau_{ei,max} \sin(\theta_{grid} - \theta_{gen}) = \tau_1 = \tau_{grid} - \tau_{el-remain}$$

$$J_{gen} \ddot{\theta}_{gen} + K_D (\dot{\theta}_{gen} - \dot{\theta}_{grid}) + \tau_{ei,max} \sin(\theta_{gen} - \theta_{grid}) = \tau_2 = \tau_{gen}$$

Trip due to Generator Pole Slip (Simulated)

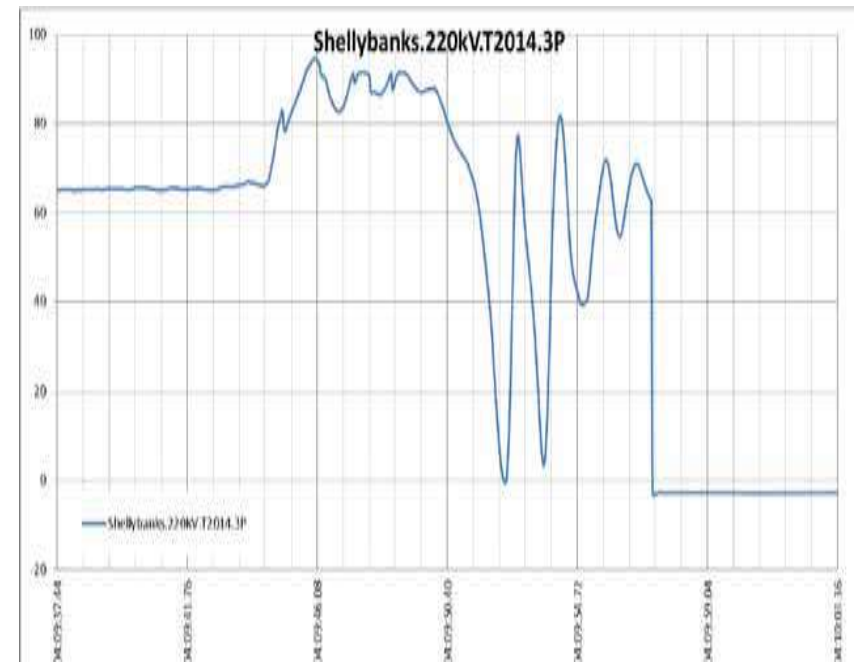


By reducing the wrong setting of the maximum load from 470MW to 461MW the unit becomes compliant to the grid code. Unfortunately, until this modification is done the Under-Excitation Limits had to be reduced by 45MVAR which costs €2700 per day!

Real Event, Poolbeg CT 15 @ 65 MW



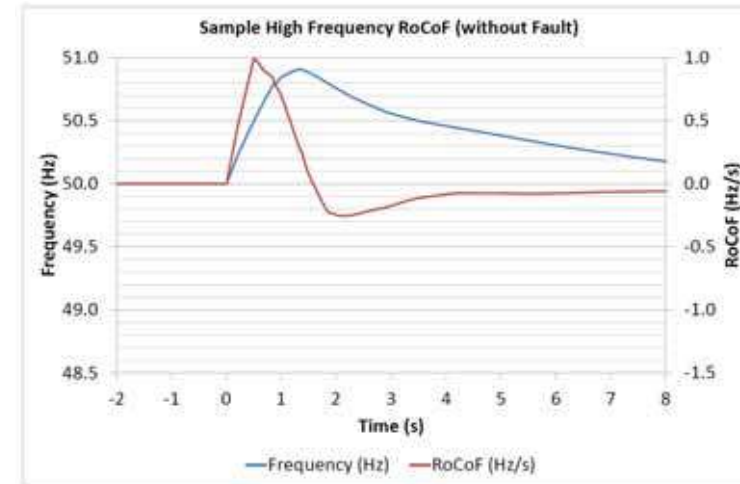
Fuel: Natural gas
Capacity: 480MW
Commissioned: 1994, 1998-99
Technology: Combined Cycle Gas Turbine (CCGT)



Real Event, North Wall, Trip on reverse power



County: Dublin
Fuel types: Oil; Gas
Capacity: 106 MW
Commissioned: 1982

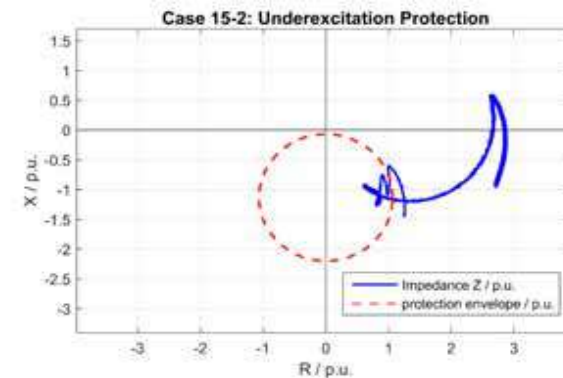
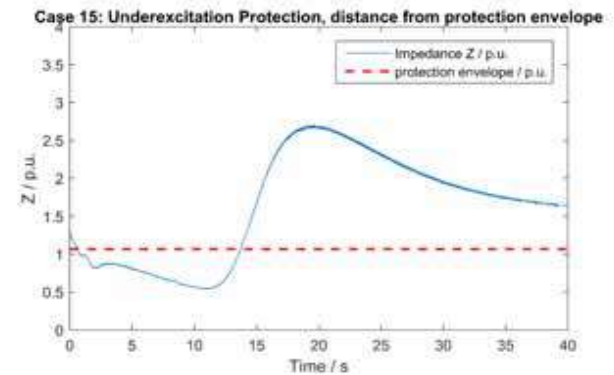


During RoCoF tests a frequency rise signal was injected. The unit, seeing a frequency rise closed the control valves and went into reverse power and tripped

Trip on Under excitation Protection (Simulation by Injection)



Lough Ree Power, Peat burning boiler, Steam Turbine, 100MW



Enerlyzer Software with CMC356



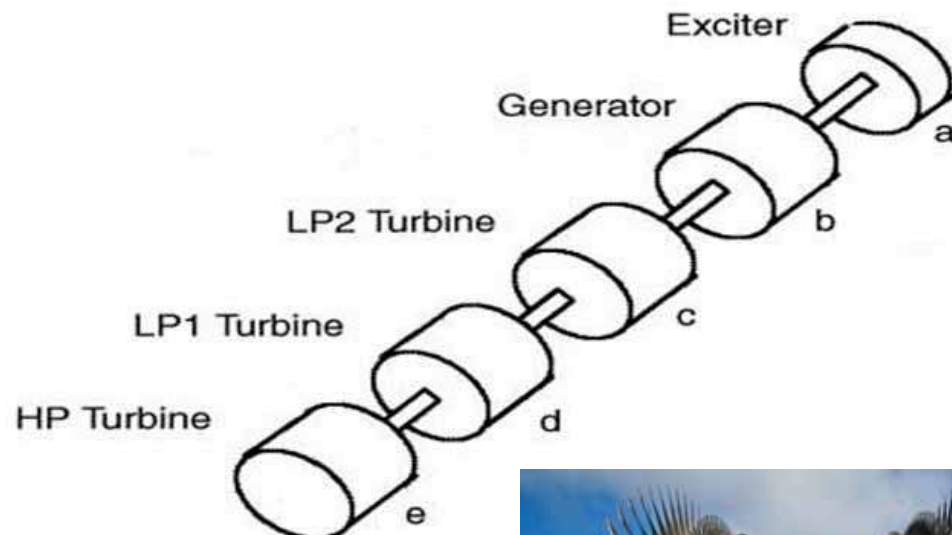
https://www.omicronenergy.com/fileadmin/_processed_/d/b/csm_Protection-Troubleshooting-CMC-TU-EnerLyzer-gallery_c616a4c1b0.jpg

The relevant protection functions, resulting in trips, for RoCoF of 'A' and 'B' systems are as follows:

- [59.1] Over Voltage
- [59.2] Over Voltage
- [78] Pole Slipping
- [24G] Generator Overfluxing
- [46.1] Load Unbalance, NPS
- [21] Minimum Impedance
- [40.1] Under Excitation
- [81.2] Under Frequency 2
- [81.3] Under Frequency 3
- [27/51] Voltage Controlled Over Current

The Comtrade files were played into an ABB REG650 ied (intelligent electronic device), using the Advanced Transplay module. The REG650 relay was configured, and tested, using secondary injection with an Omicron CMC356 relay test module and associated software, prior to the Comtrade file playbacks.

Mechanical Components



- Couplings
- Rotors and shafts
- Turbine blades and roots
- Generator rotor end bells

Mechanical Analysis, Moneypoint Generating Station



Fuel: Coal and Oil

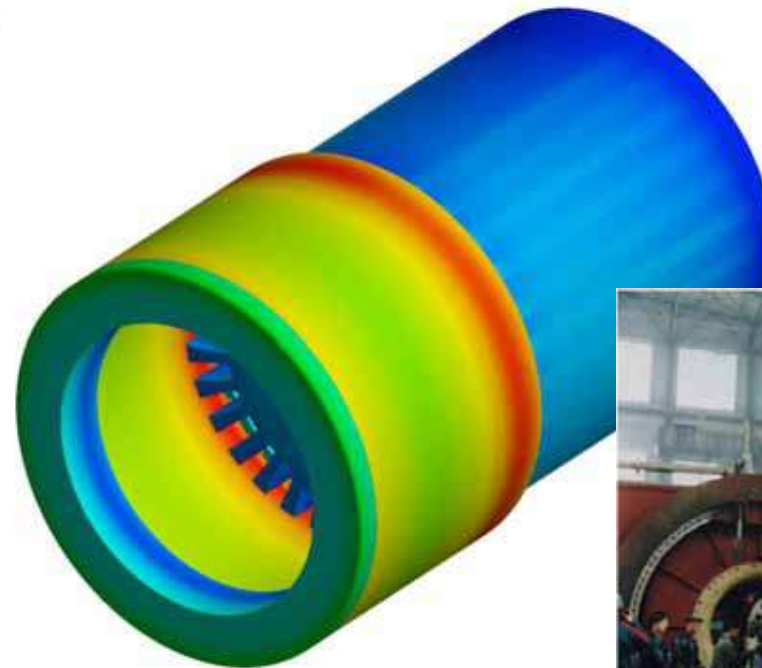
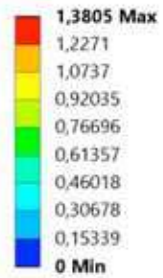
Capacity: 915 MW

Commissioned: 1985, 1986 and 1987

Technology: 3 x Steam Turbines

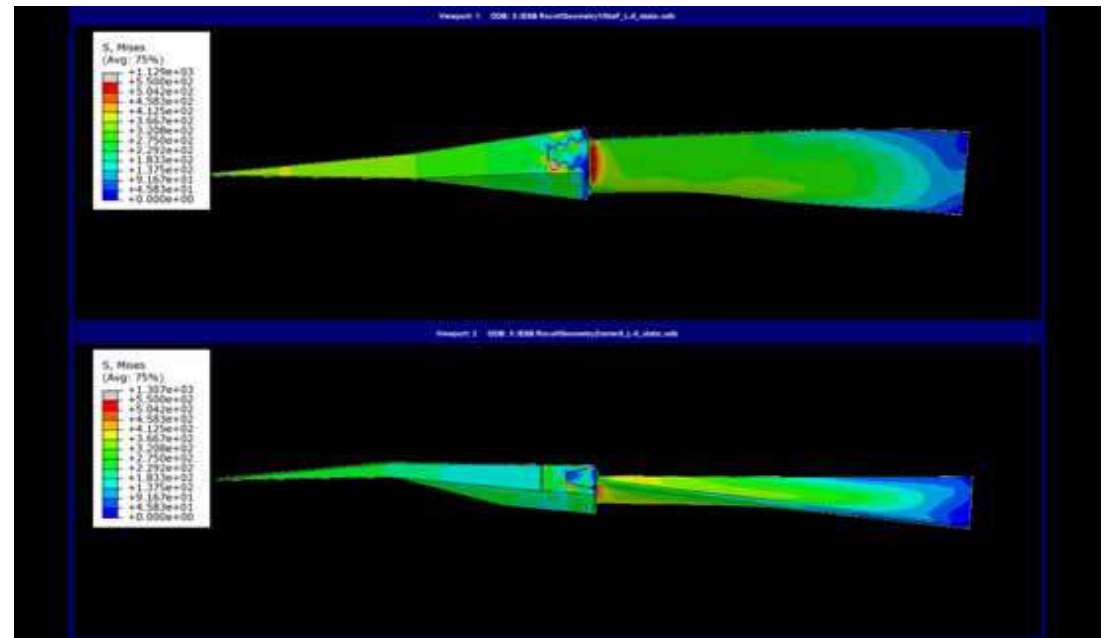
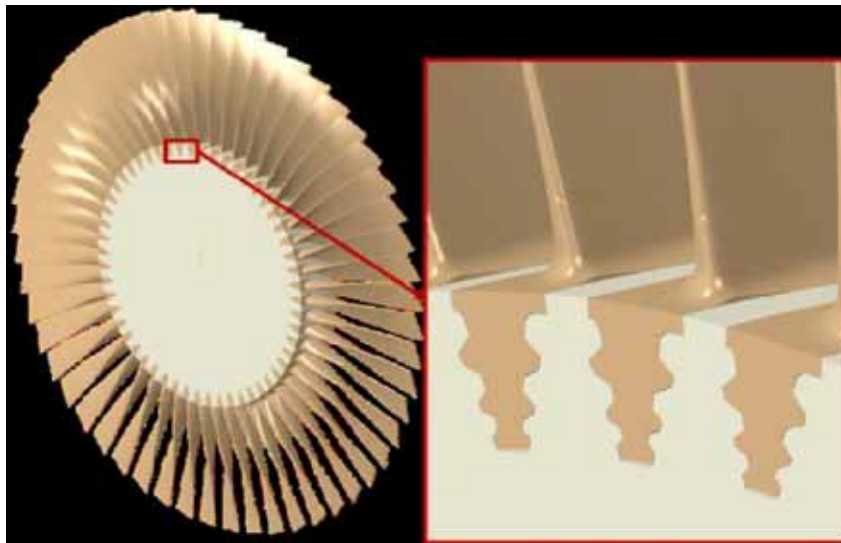
Stress on Rotor End Bell

Typ: Gesamtverformung
Einheit: mm



TUV Report, Moneypoint, Generator Rotor

Mechanical analysis: Blade oscillations and stresses



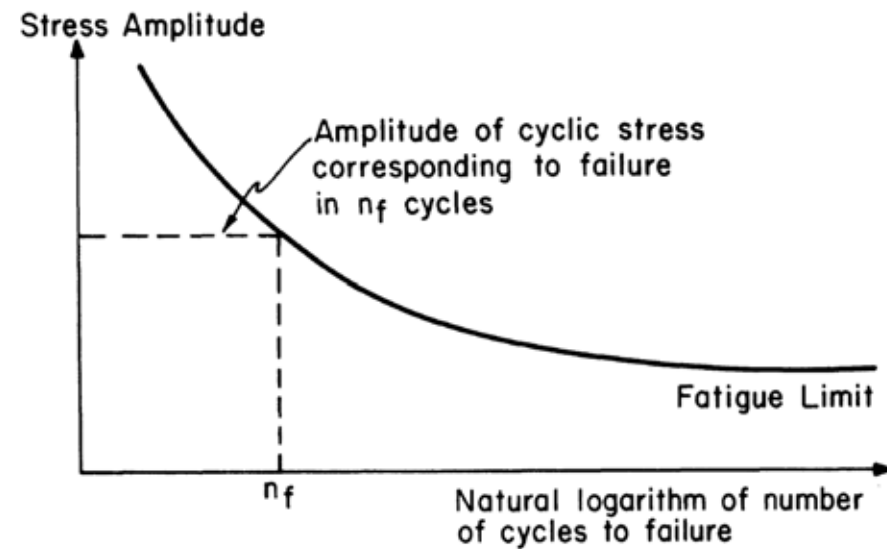
TUV Report, Moneypoint Steam Turbine 305MW

Risks related to mechanical integrity

Torsional oscillations can create stresses to:

- Couplings
- Rotors and shafts
- Turbine blades
- Generator rotor end bells
- Generator stator end windings

Woehler Curve (SN Curve):



ROCOF Event

Further loss of Electrical Power Generations



Cascade Tripping Event



Load Shedding in the system



System Brown/Black Out



Mech/Elec Integrity Consequences of CoF Event

Reduced Component Life Time



Consequential Machine Damage



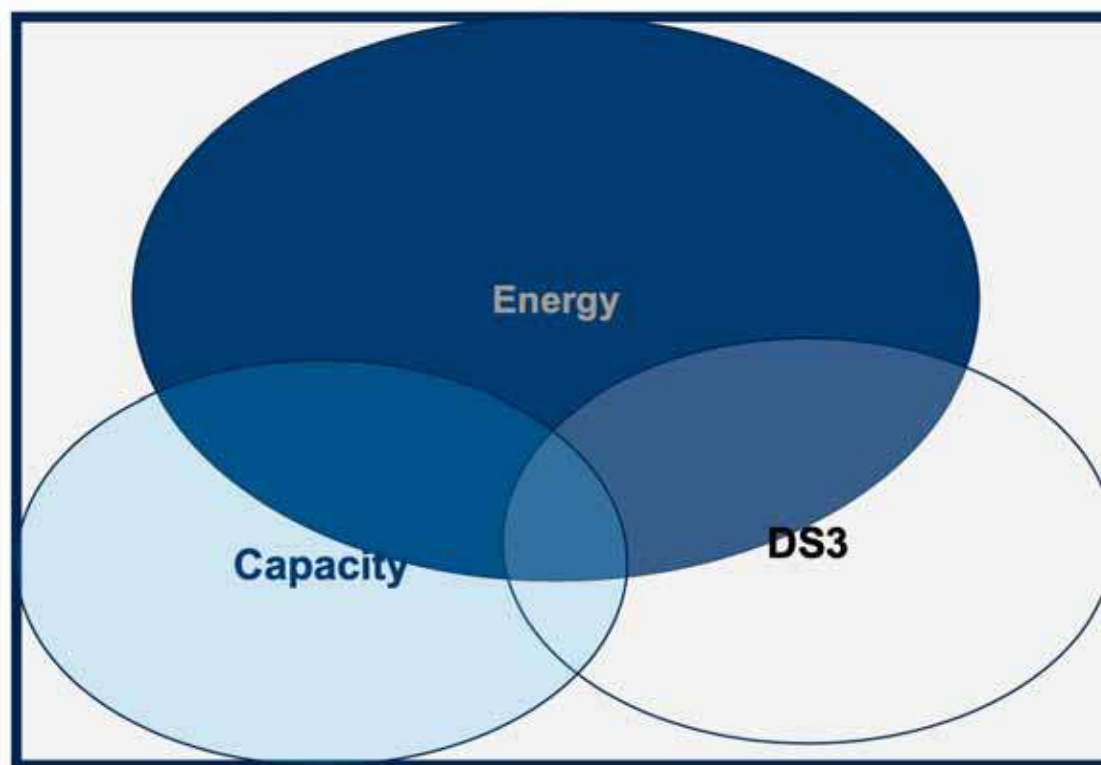
Decreased overhaul intervals and
Increased Inspection Requirements



Forced Outage



We need inertia



Performance Categorization



www.eirgridgroup.com/site-files/library/EirGrid/DS3-System-Services-Interim-Protocol-Document-Version-2.1.pdf

Declaration	Fast Frequency Response	Ramping Margin 1 Hour	Ramping Margin 3 Hour	Ramping Margin 8 Hour	Dynamic Reactive Response	Fast Post Fault Active Power Recovery	Automatic Voltage Regulation	Current Fuel
EDIL Acronym	FFR	RM1	RM3	RM8	DRR	FPFAPR	AVR	FUEL
Description	Fast Frequency Response in MW	Ramping Margin 1-3 Hours in MW	Ramping Margin 3-8 Hours in MW	Ramping Margin 8-16 Hours in MW	Ability to provide Dynamic Reactive Response	Ability to provide Fast Post Fault Active Power Recovery	Ability to Act Under AVR	Current Fuel Being Used
Framework Agreement term	Declared FFR	Declared RM1	Declared RM3	Declared RM8	Declared DRR	Declared FPFAPR	Declared Automatic Voltage Regulator Status	No standalone term – used in average Availability calculation

DS3 - System Services

System Service	Acronym	Compliance Requirements for Existing Harmonised Ancillary Service Providers using existing contract values	Compliance Requirements for Existing Harmonised Ancillary Service Providers proposing to use revised contract values	Compliance Requirements for New Providers that have not previously provided Harmonised Ancillary Services equivalent to DS3 System Service
Synchronous Inertial Response	SIR	Must be a Synchronous Machine. H Constant must be confirmed.	Must be a Synchronous Machine. If proposing to change H Constant, the change must be confirmed with TSO.	Must be a Synchronous Machine. H Constant must be confirmed with TSO.
Fast Frequency Response	FFR	Services will be procured through trials for Interim Arrangements. Compliance Requirements to be determined as part of trials.	Services will be procured through trials for Interim Arrangements. Compliance Requirements to be determined as part of trials.	Services will be procured through trials for Interim Arrangements. Compliance Requirements to be determined as part of trials.
Dynamic Reactive Response	DRR			
Fast Post-Fault Active Power Recovery	FPFAPR			
Primary Operating Reserve	POR	Compliance assessment will be based on historical data. No additional testing will be required.	Compliance assessment will be based on historical data if it exists for newly proposed contract values (revised either up or down). Outside of these values, additional Frequency Injection Testing or testing using Dispatch instructions as appropriate may be required as determined by the TSO.	Compliance assessment based on Frequency Injection Testing or testing using Dispatch instructions as appropriate may be required as determined by the TSO.
Secondary Operating Reserve	SOR			
Tertiary Operating Reserve 1	TOR1			
Tertiary Operating Reserve 2	TOR2			
Ramping Margin 1 Hour	RM1	Compliance assessment will be based on historical data. No additional testing will be required.	Compliance assessment will be based on historical data if it exists for newly proposed contract values (revised either up or down). Outside of these values, additional testing may be required involving Dispatch	Compliance assessment based on testing involving Dispatch instructions may be required as determined by the TSO.
Ramping Margin 3 Hour	RM3			
Ramping Margin 8 Hour	RM8			
Replacement Reserve (De-Synchronised)	RRD			



Energy for
generations

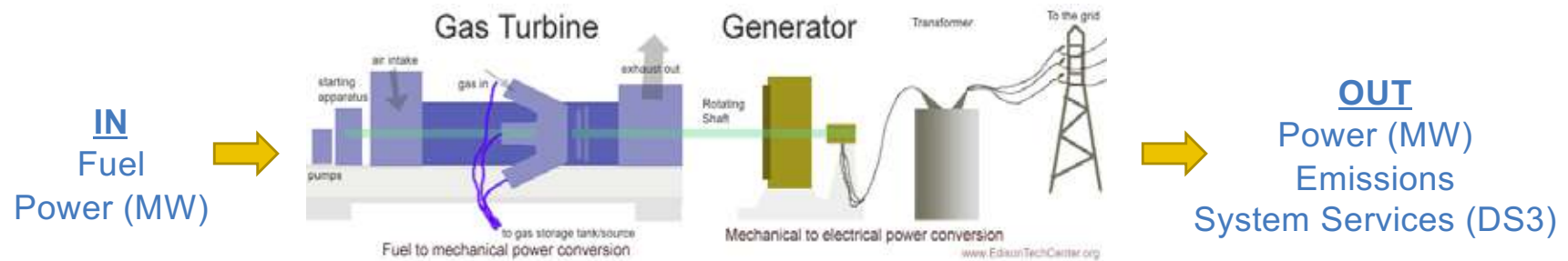
Moneypoint Synchronous Condenser

Katie Wall, Lead Engineer

June 2022



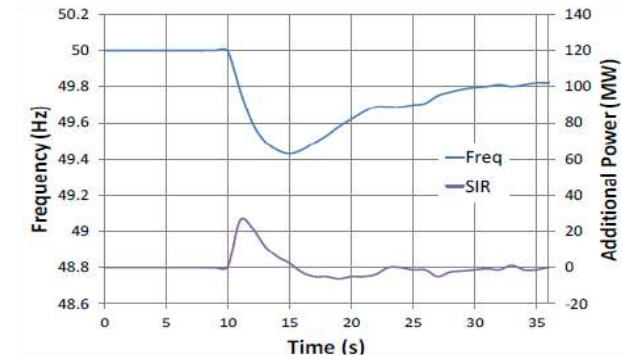
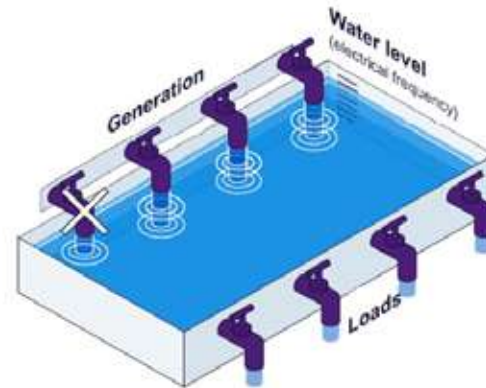
What is a Synchronous Condenser



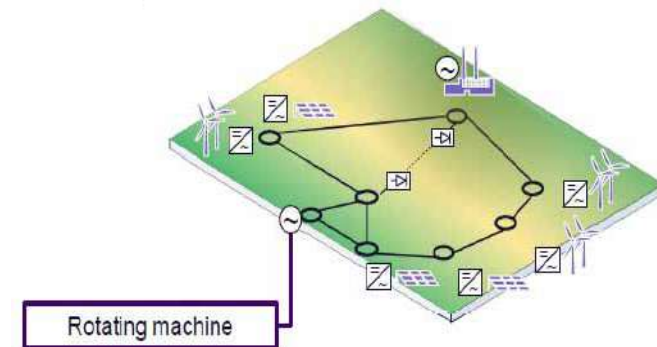
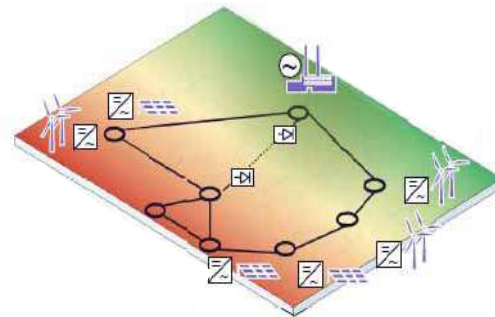
NO FUEL, NO COMBUSTION, NO EMISSIONS

Images Reference: EdisonTechCentre.org

- Inertia (SIR)

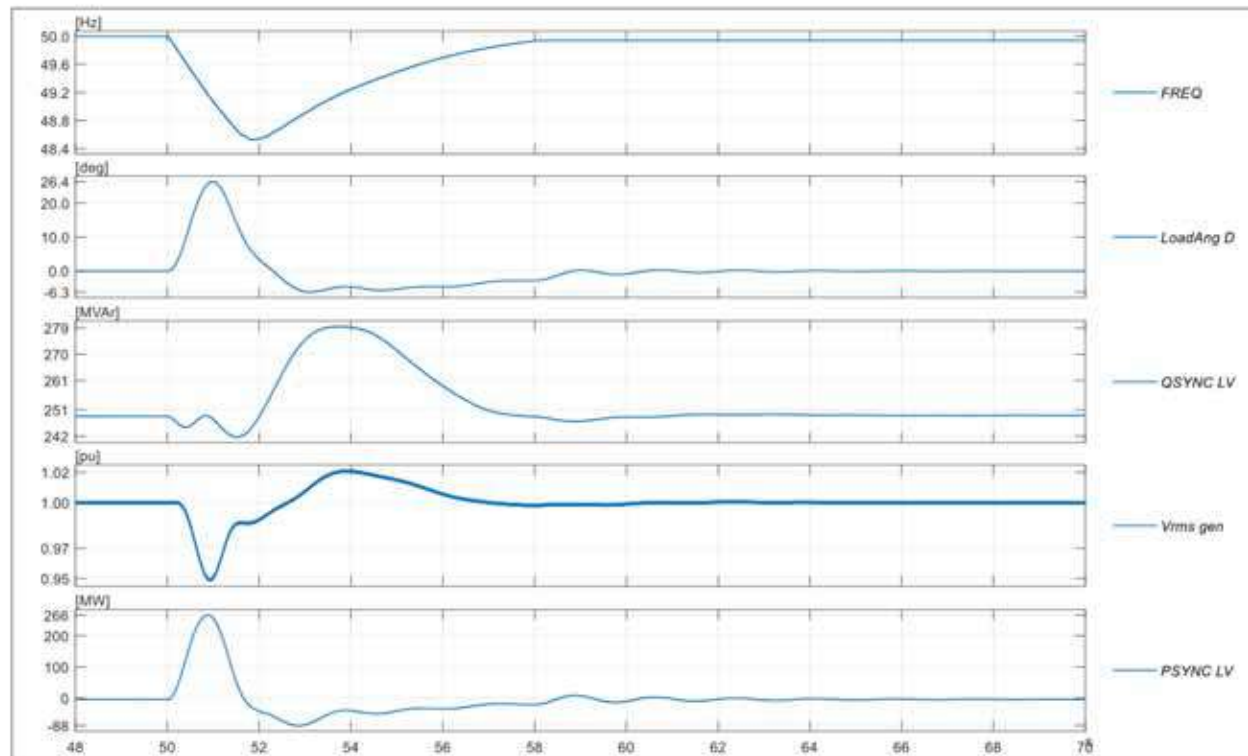


- Reactive Power (SSR)



Images Reference: Siemens Energy, 2020

Response of Synchronous Condenser to a frequency event



Synchronous Condenser & Flywheel

Synchronous Condenser

- Inertia 512 MWs

Flywheel

- Inertia 3488 MWs

Total Inertia = 4000 MWs
≅ 2 x existing MP units



Images Reference: Siemens Energy, 2020

Synchronous Condenser

Siemens SGen5 1200A 2P

- +260 MVar (capacitive/lagging),
-111MVar (inductive/leading)
- 970 MVA short circuit power
- Air Cooled
- Rotor weight = 67,160 kg



Syncon Rotor

Flywheel

Design based on existing gen rotors / LP turbines

- 4 m long, 2.2 m diameter
- Monoblock metal
- Rotor weight = 126,300 kg
- Water cooled
- Operates in Vacuum



Largest flywheel installation in world



Delivery to site

Flywheel forged in Italy, final machining & assembly in Mulheim, Germany

SynCon manufactured in Erfurt, Germany

Barge to Rotterdam

Cargo ship to Foynes, Co. Limerick

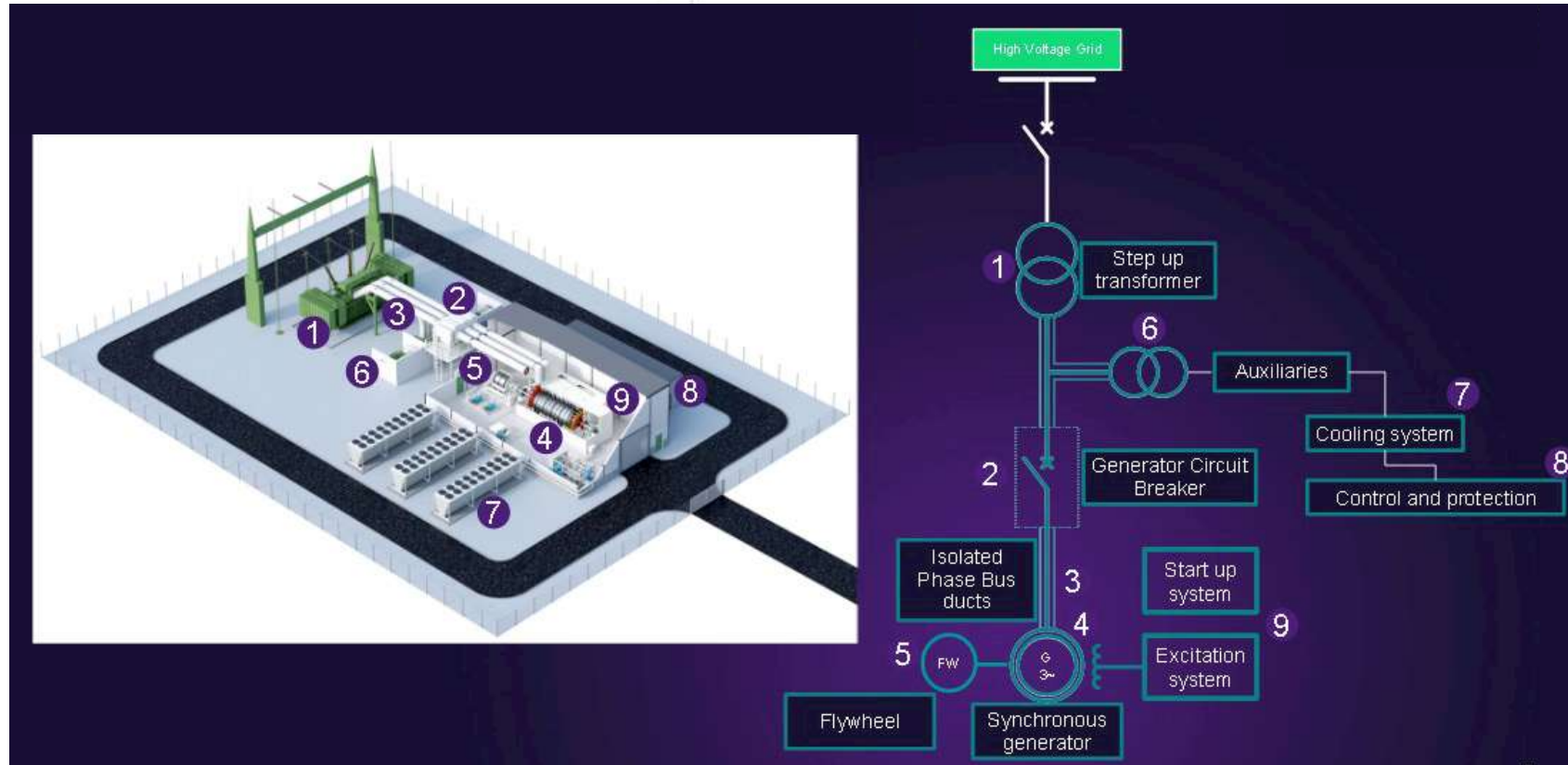
Barge to Moneypoint jetty



Delivery to site



Moneypoint SynCon Layout



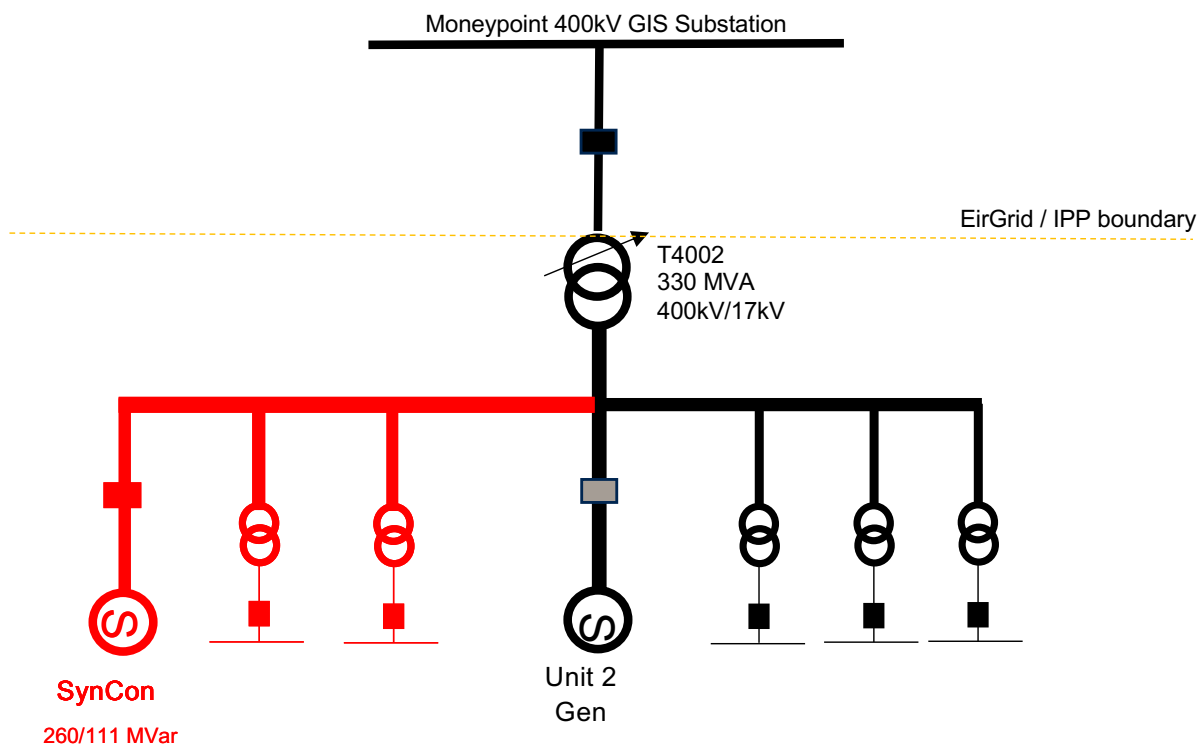
Images Reference: Siemens Energy, 2020

Shared Grid Connection with MP Unit 2

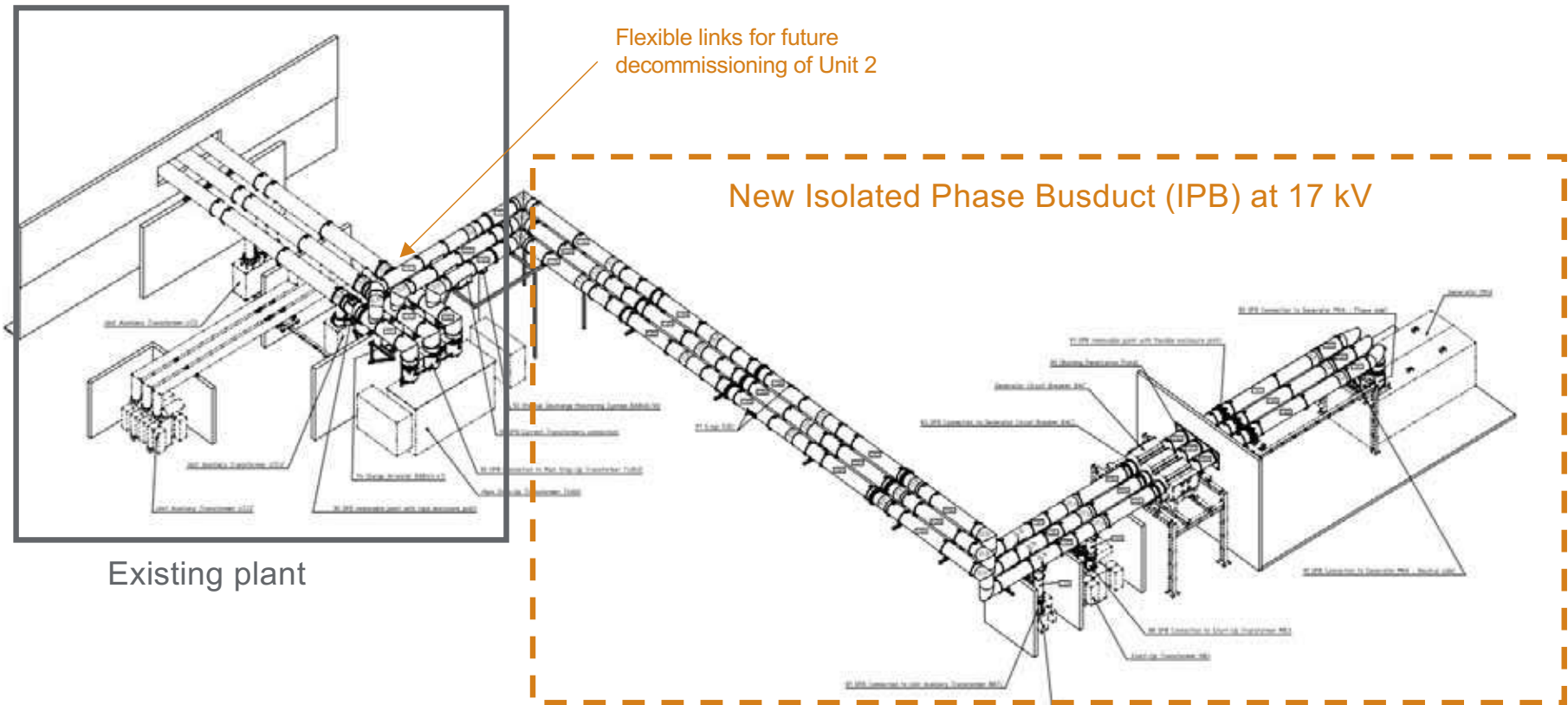


Note: MP2 & SynCon interlocked

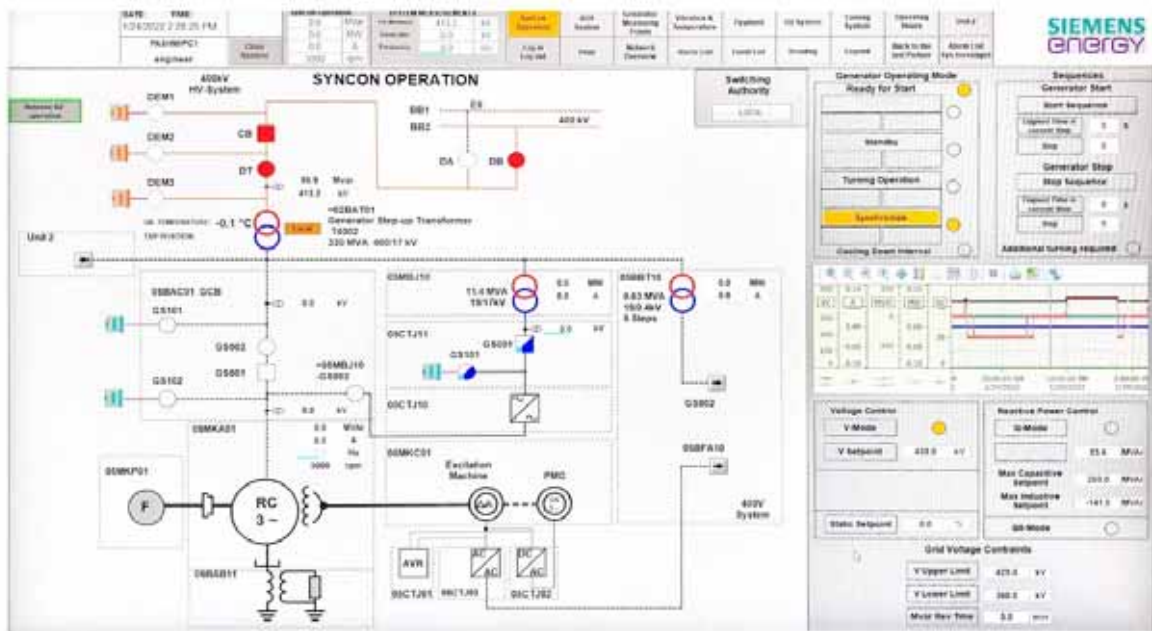
Parallel Operation not permitted



Shared Grid Connection with MP Unit 2

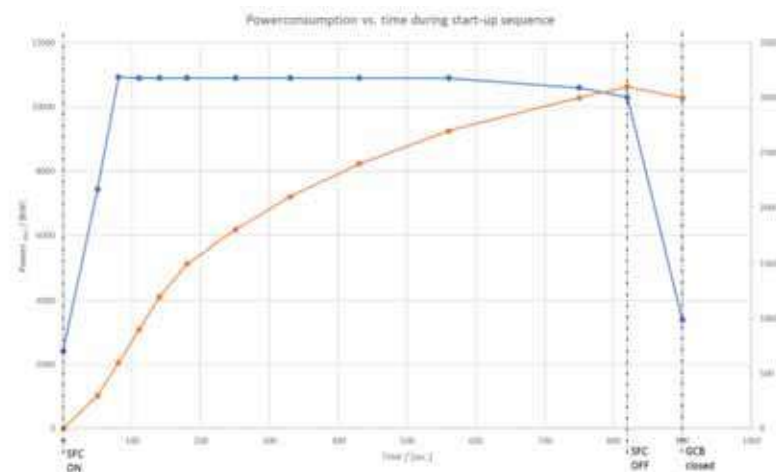


Remotely Operated from Dublin



15 mins start-up (11 MW import)

4 MW – 5 MW continuous operation depending on MVar output



De-sync & coast down = 8 hours (can use SFC for braking to reduce this)

Progress & Programme



Planning
Permission Aug '20 ✓



EPC Contract
April '21 ✓



Detailed Design
May '21 – April '22 ✓



Site Mobilisation
Sept '21 ✓



SynCon & Flywheel
delivery
April '22 ✓



14 FATs completed
Sept '21 - April '22 ✓



Centreline
Concrete Pour
March '22 ✓



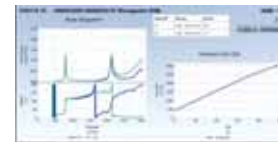
Piling
Dec '21 ✓



Civil work finalising
May '22 ✓



Cold commissioning
June – July '22 ✓



Hot commissioning
& Grid Code
Testing



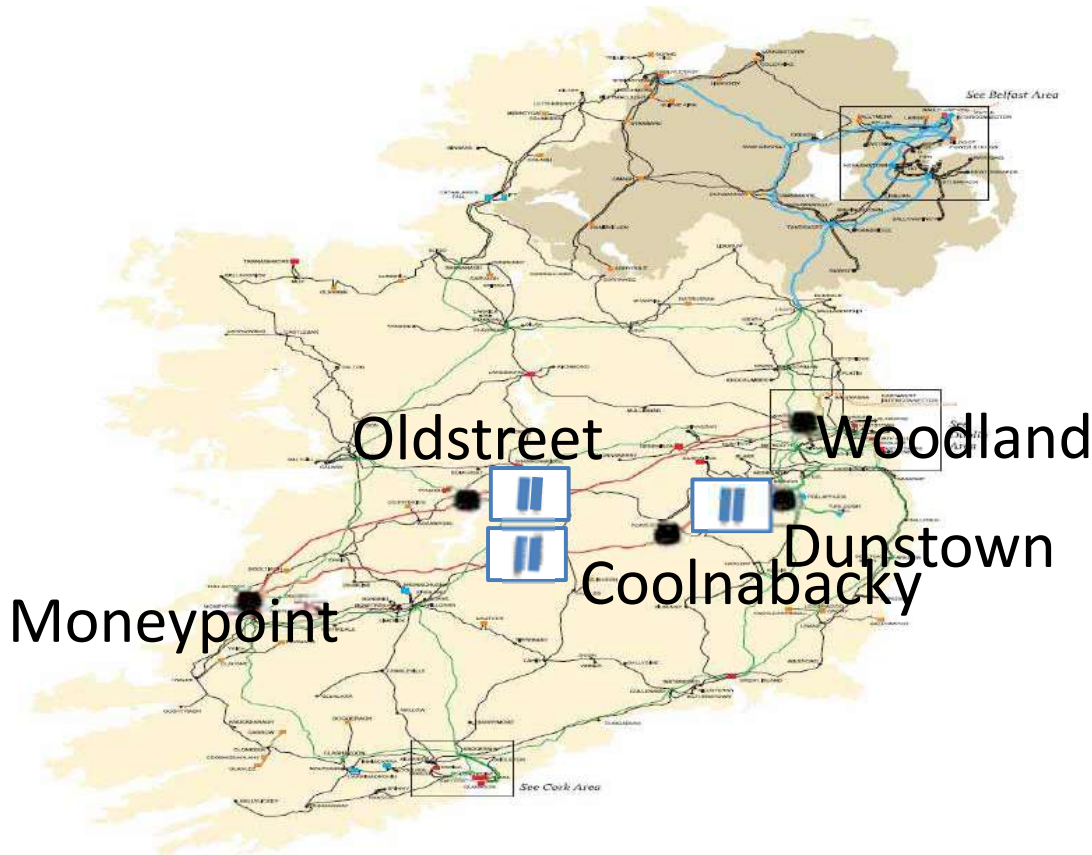
Commercially Operational
Oct

Conclusion



[Siemens Energy Ireland & Siemens Energy Germany, Time-lapse - April 2022 \(vimeo.com\)](#)

Three 400kV Series Capacitors close to MP, Tender Issue Q1 2023; Energisation 2025



Oldstreet - Woodland 400kV Series Capacitor

Compensation Level		70%
Location	Oldstreet substation	
Capacitance	μF	111
Impedance	Ω	28.6
Reactive Power Rating	Mvar	676

Moneypoint - Coolnabacky 400kV Series Capacitor

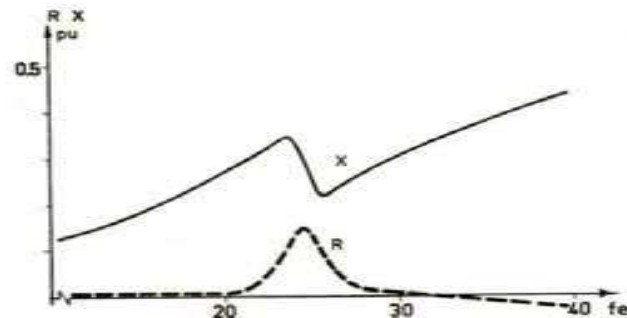
Compensation Level		54%
Location	127km from Moneypoint	
Capacitance	μF	111
Impedance	Ω	28.6
Reactive Power Rating	Mvar	676

Coolnabacky - Dunstown 400kV Series Capacitor

Compensation Level		70%
Location	Dunstown substation	
Capacitance	μF	315
Impedance	Ω	10.1
Reactive Power Rating	Mvar	239

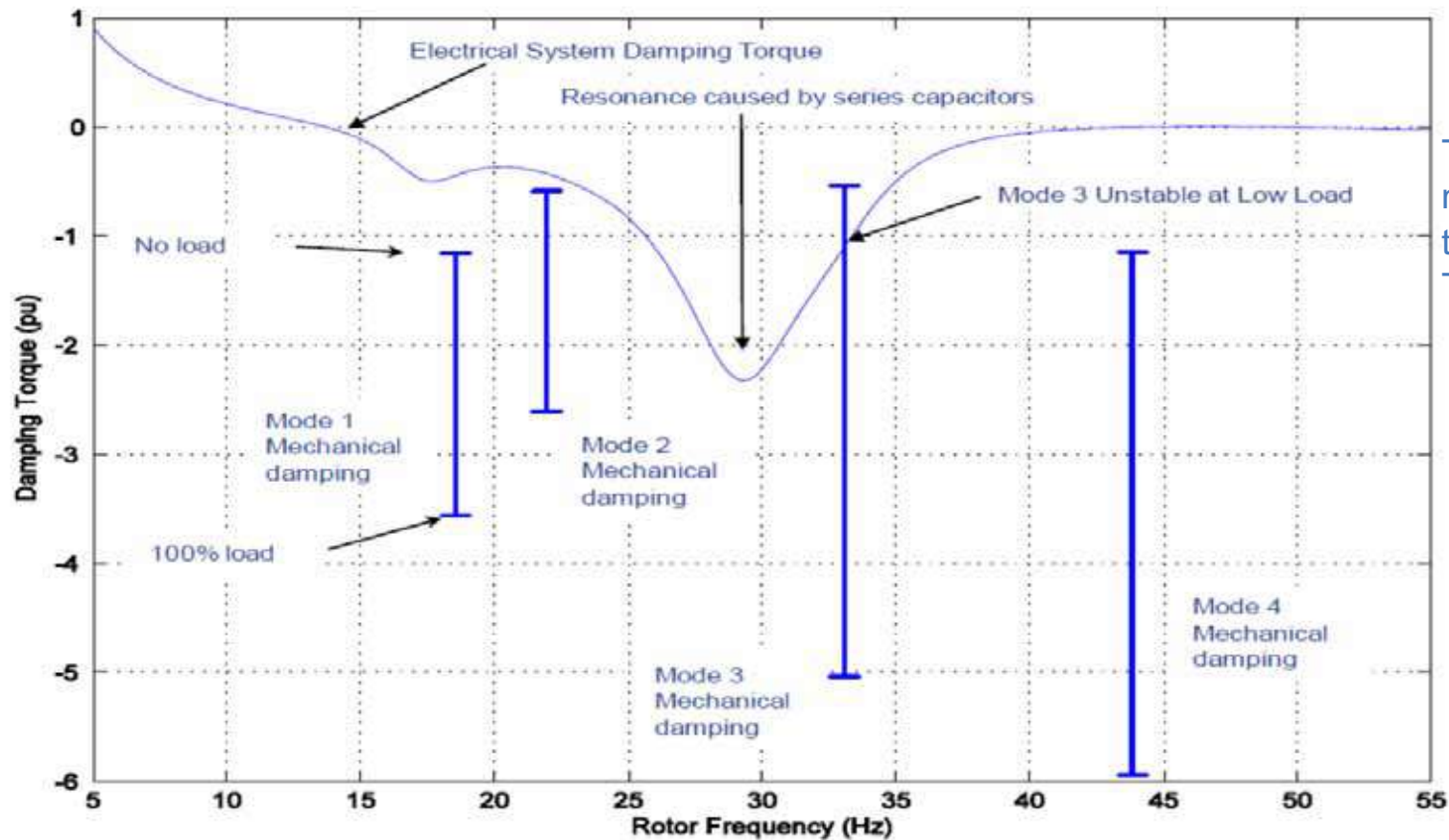
Sub Synchronous Resonance (SSR) Series capacitors change 'impedance quality' of electrical system

- Series capacitors introduce series and parallel resonances in the sub-synchronous range (less than 50Hz)
- The resonances can interact with shafts of turbines, or the control system of converters



- Risk of interaction depends also upon mechanical and electrical characteristics of the generator

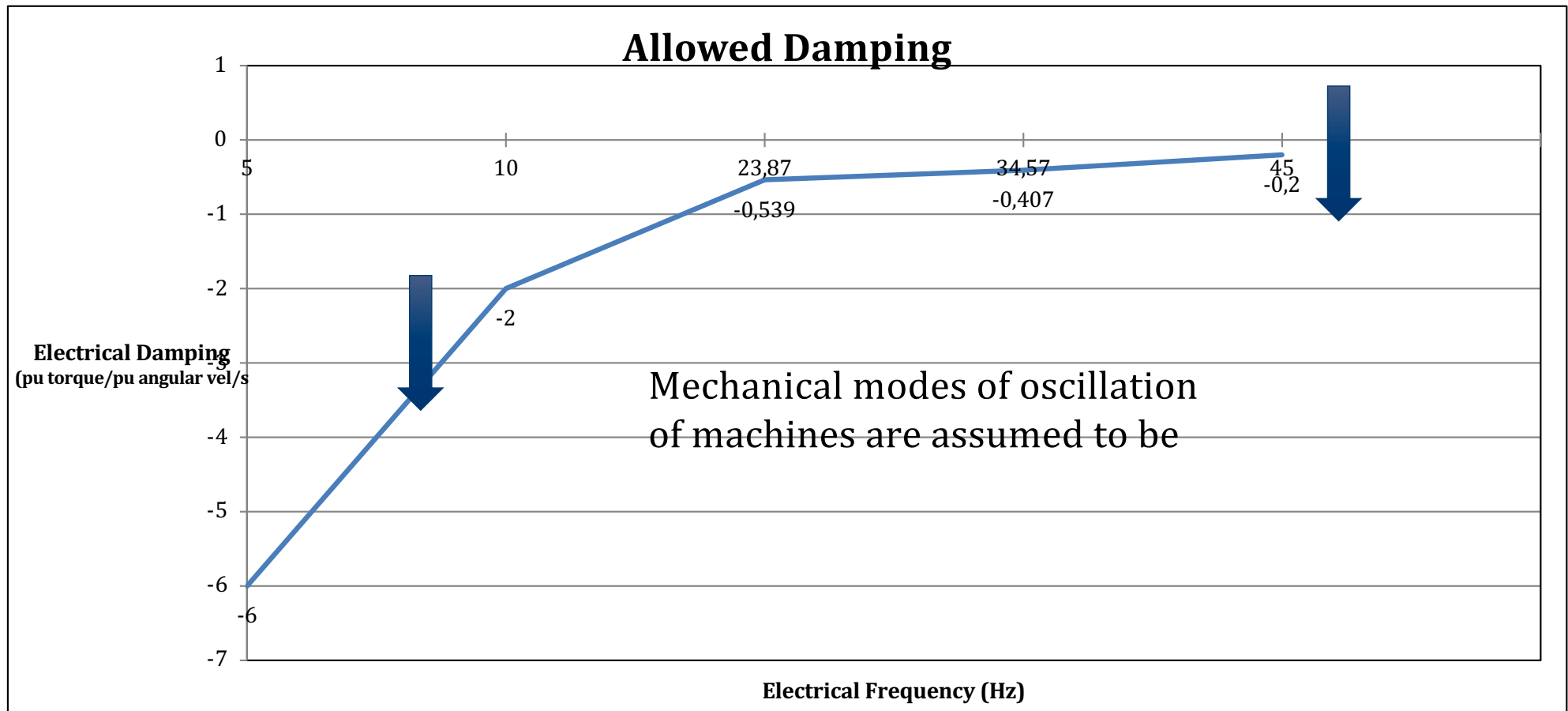
SSR Interaction depends on mechanical characteristics of machines



These Generator modes shown are of the MP Steam Turbine units

TSO Criteria for SSR Mitigation

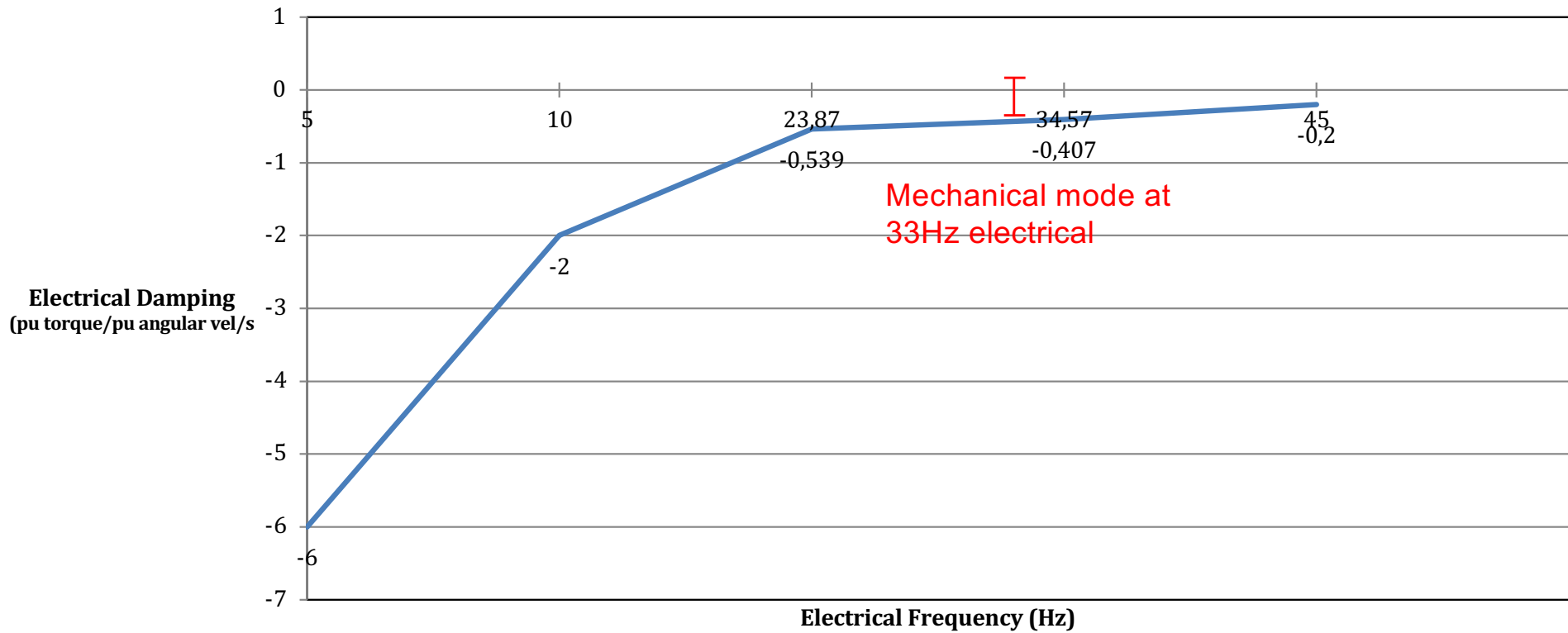
Controls negative electrical damping due to series capacitors...



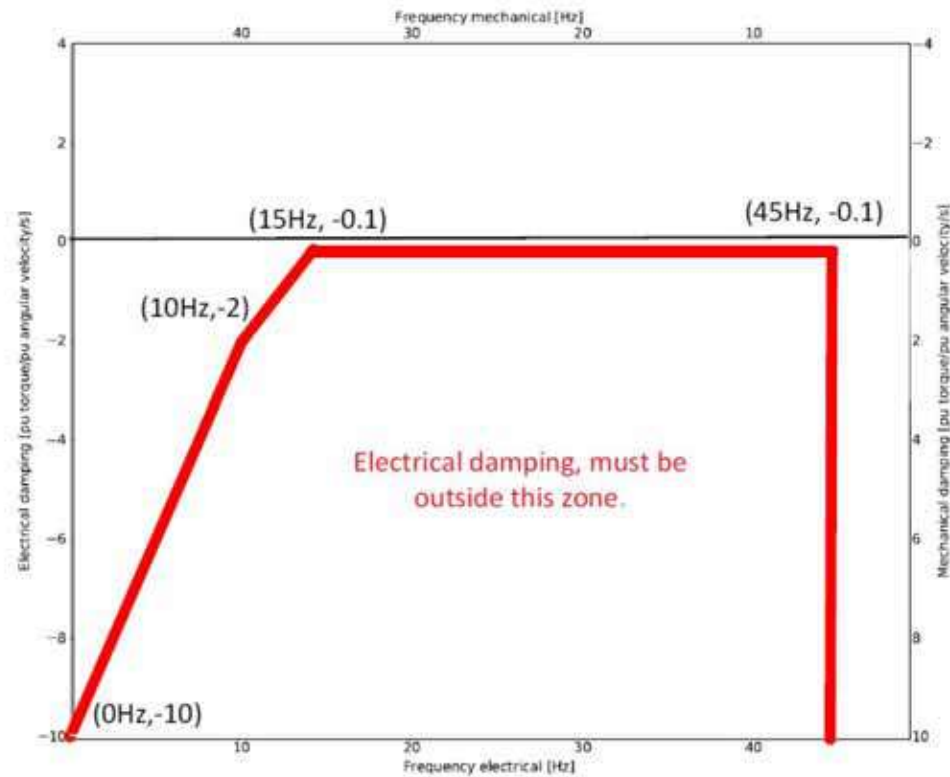
MP Synchronous Condenser

One mechanical mode of oscillation of concern reported at 33Hz with low mechanical damping...

Allowed Damping

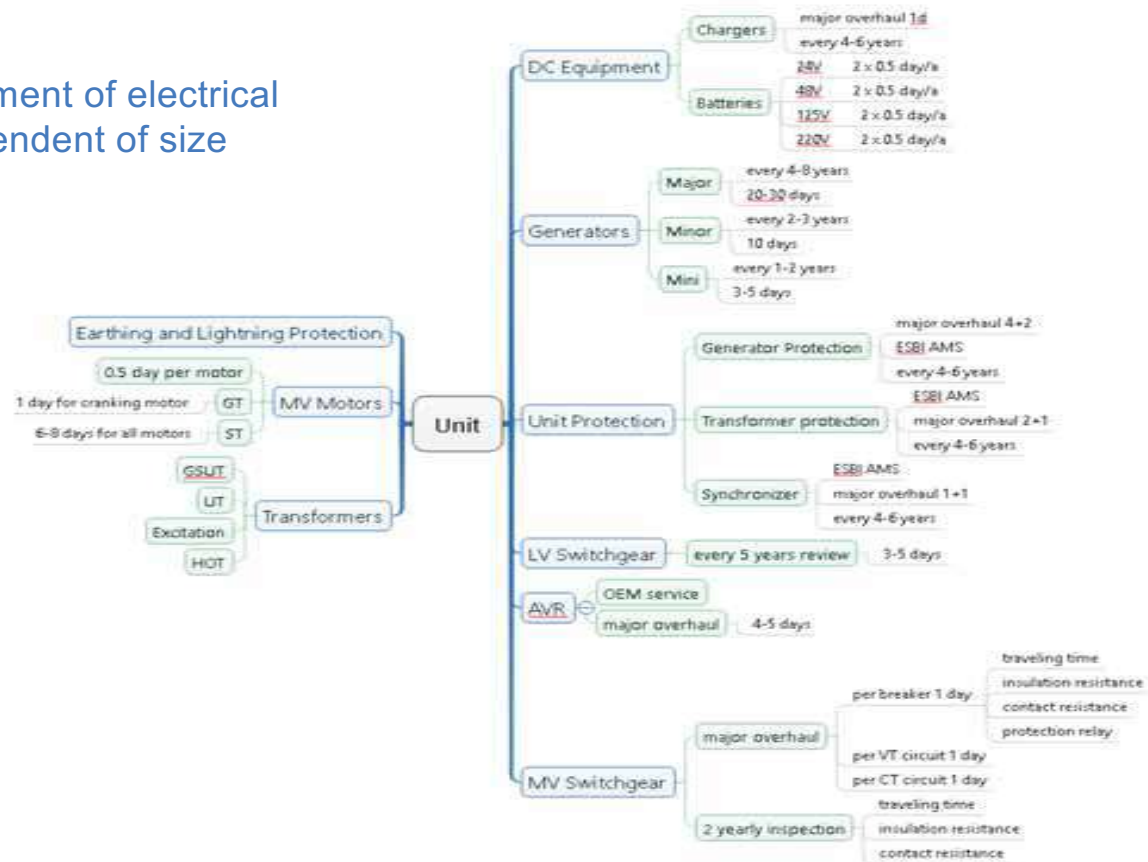


Series Compensation, Damping

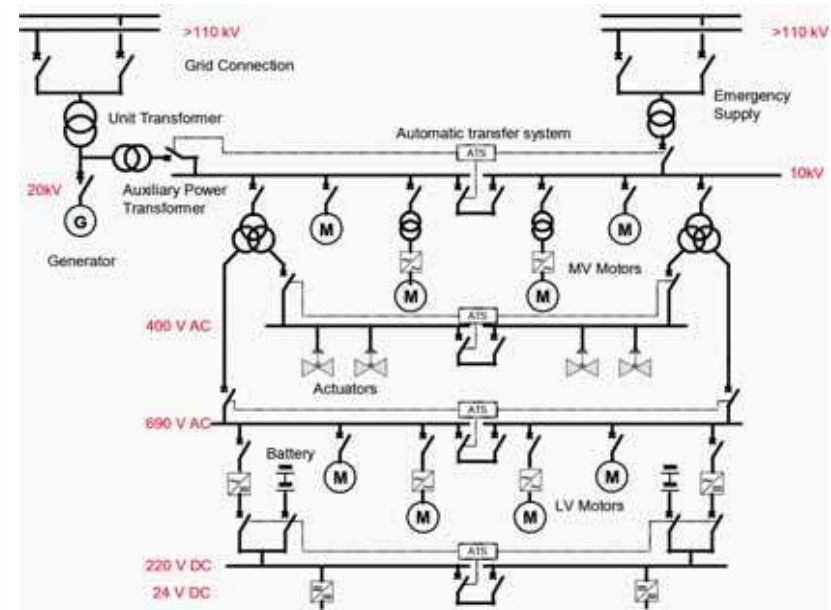
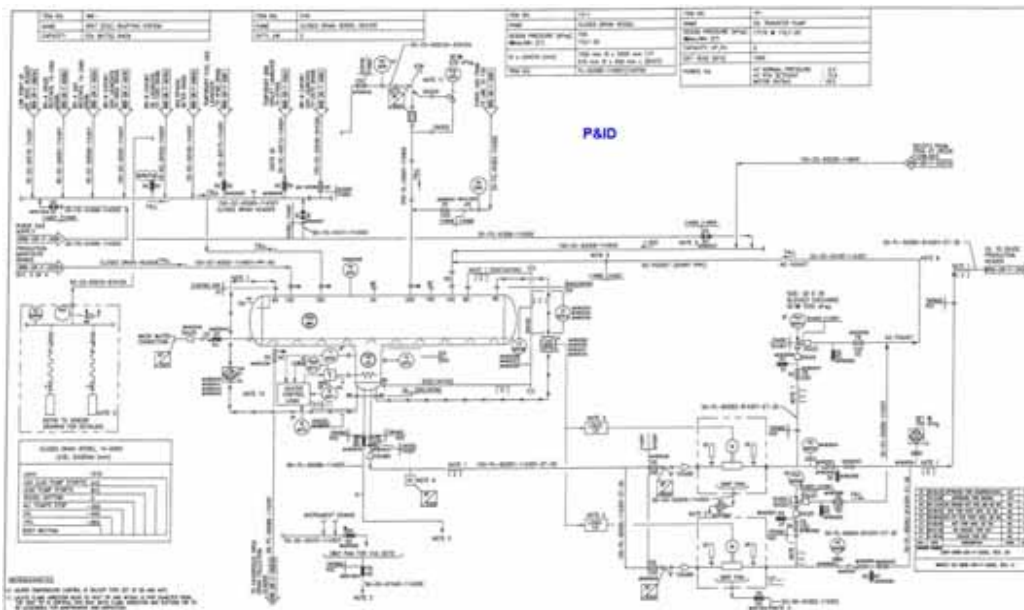


Additional Assets require Skilled Personnel:

Maintenance requirement of electrical assets is often independent of size



Personnel Development: Understanding of components within Generating Assets



Personnel Development: Understanding of theory

Models for the transient stability of conventional power generating stations connected to low inertia systems

Marios Zarifakis^{1,2}, William T. Coffey², Yuri P. Kalmykov³ and Serguey V. Titov⁴

¹Electricity Supply Board, Generation, Asset Management, Dublin 2, Ireland

²Department of Electronic and Electrical Engineering, Trinity College, Dublin 2, Ireland

³Laboratoire de Mathématiques et Physique (EA 4217), Université de Perpignan Via Domitia, F-66860, Perpignan, France

⁴Kotel'nikov Institute of Radio Engineering and Electronics of the Russian Academy of Sciences, Vvedenskii Square 1, Fryazino, Moscow Region, 141120, Russia

Abstract

An ever-increasing requirement to integrate greater amounts of electrical energy from renewable sources especially from wind turbines and solar photo-voltaic installations exists and recent experience in the island of Ireland demonstrates that this requirement influences the behaviour of conventional generating stations. One observation is the change in the electrical power output of synchronous generators following a transient disturbance especially their oscillatory behaviour accompanied by similar oscillatory behaviour of the grid frequency, both becoming more pronounced with reducing grid inertia. This behaviour cannot be reproduced with existing mathematical models indicating that an understanding of the behaviour of synchronous generators, subjected to various disturbances especially in a system with low inertia requires a new modelling technique. Thus two models of a generating station based on a double pendulum described by a system of coupled nonlinear differential equations and suitable for analysis of its stability corresponding to infinite or finite grid inertia are presented. Formal analytic solutions of the equations of motion are given and compared with numerical solutions. In particular the new finite grid model will allow one to identify limitations to the operational range of the synchronous generators used in conventional power generation and also to identify limits, such as the allowable Rate of Change of Frequency which is currently set to $\pm 0.5\text{Hz/s}$ and is a major factor in describing the volatility of a grid as well as identifying requirements to the total inertia necessary, which is currently provided by conventional power generators only, thus allowing one to maximise the usage of grid connected non-synchronous generators e.g. wind turbines and solar photo-voltaic installations.

Now we introduce

$$c_{nq}^{\pm n} = \theta_1^n \theta_2^n r_1^n r_2^n, \quad n=0,1,2,\dots, \quad q=0,\pm 1,\pm 2,\dots \quad (\text{C.2})$$

where $r_i = e^{-\alpha_i t}$. Then, noting Eqs. (C.1) and (C.2), we have

$$\begin{aligned} \frac{d}{dt} c_{nq}^{\pm n} = & -(\beta_1 n_1 + \beta_2 n_2) c_{nq}^{\pm n} + \beta_1 n_1 c_{n-1,q}^{\pm n} + \beta_2 n_2 c_{n-1,q}^{\pm n} - i q_1 c_{nq}^{\pm n} - i q_2 c_{nq}^{\pm n} \\ & + \bar{F}_1 n_1 c_{n-1,q}^{\pm n} + \frac{i}{2} \bar{G}_1 n_1 (c_{n-1,q-1}^{\pm n} - c_{n-1,q+1}^{\pm n}) + \bar{F}_2 n_2 c_{n-1,q}^{\pm n} + \frac{i}{2} \bar{G}_2 n_2 (c_{n-1,q-1}^{\pm n} - c_{n-1,q+1}^{\pm n}). \end{aligned} \quad (\text{C.3})$$

Thus on introducing column vectors $C_n(t)$ defined as

$$C_1(t) = \begin{pmatrix} c_{10} \\ c_{11} \\ c_{1-1} \end{pmatrix}, \quad C_2(t) = \begin{pmatrix} c_{20} \\ c_{21} \\ c_{2-1} \end{pmatrix}, \dots, \quad C_n(t) = \begin{pmatrix} c_{n,n} \\ c_{n,n-1} \\ \vdots \\ c_{n,-n+1} \end{pmatrix} \quad (\text{C.4})$$

where the subvectors are

$$c_{n,n}(t) = \begin{pmatrix} \vdots \\ c_{n,n}^{\pm 1}(t) \\ c_{n,n}^{\pm 2}(t) \\ c_{n,n}^{\pm 3}(t) \\ \vdots \end{pmatrix}, \quad (\text{C.5})$$

it follows that the differential-recurrence Eq. (C.3) can be transformed into the matrix three-term recurrence equation (B.4), namely,

$$\frac{d}{dt} C_n(t) = Q_n C_{n-1}(t) + Q_n C_n(t) + Q_n^* C_{n+1}(t), \quad (\text{C.6})$$

where the matrices Q_n and Q_n^* are given by

$$Q_n = -\beta_1 \begin{pmatrix} (n-1)\mathbf{I} & -(n-1)\mathbf{I} & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & (n-2)\mathbf{I} & -(n-2)\mathbf{I} & \ddots & \vdots \\ \mathbf{0} & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \mathbf{0} & \mathbf{I} & -\mathbf{I} \\ \mathbf{0} & \dots & \mathbf{0} & \mathbf{0} & \mathbf{0} \end{pmatrix} - \beta_2 \begin{pmatrix} \mathbf{0} & \mathbf{0} & \mathbf{0} & \dots & \mathbf{0} \\ -\mathbf{I} & \mathbf{I} & \mathbf{0} & \ddots & \vdots \\ \mathbf{0} & \mathbf{0} & \ddots & \ddots & \mathbf{0} \\ \vdots & \ddots & -(n-2)\mathbf{I} & (n-2)\mathbf{I} & \mathbf{0} \\ \mathbf{0} & \dots & \mathbf{0} & -(n-1)\mathbf{I} & (n-1)\mathbf{I} \end{pmatrix} \quad (\text{C.7})$$

$$Q_n^* = -i \begin{pmatrix} q^+ & q^- & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & q^+ & q^- & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \mathbf{0} \\ \mathbf{0} & \dots & \mathbf{0} & q^+ & q^- \end{pmatrix}, \quad (\text{C.8})$$

Commercial Challenges – Price Volatility and Predictability



High Wind => Low Prices
Low Wind => High Prices

=> Caused by non-availability of conventional generation

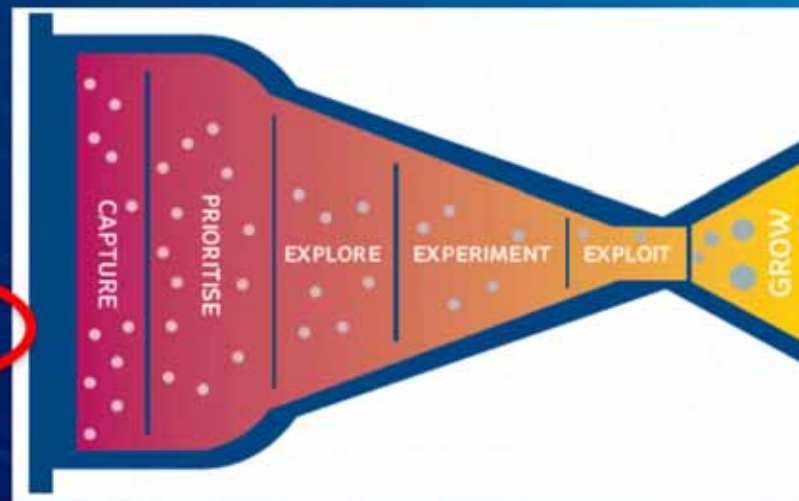
=> Technical challenge to increase availability and reliability

Last, but not least

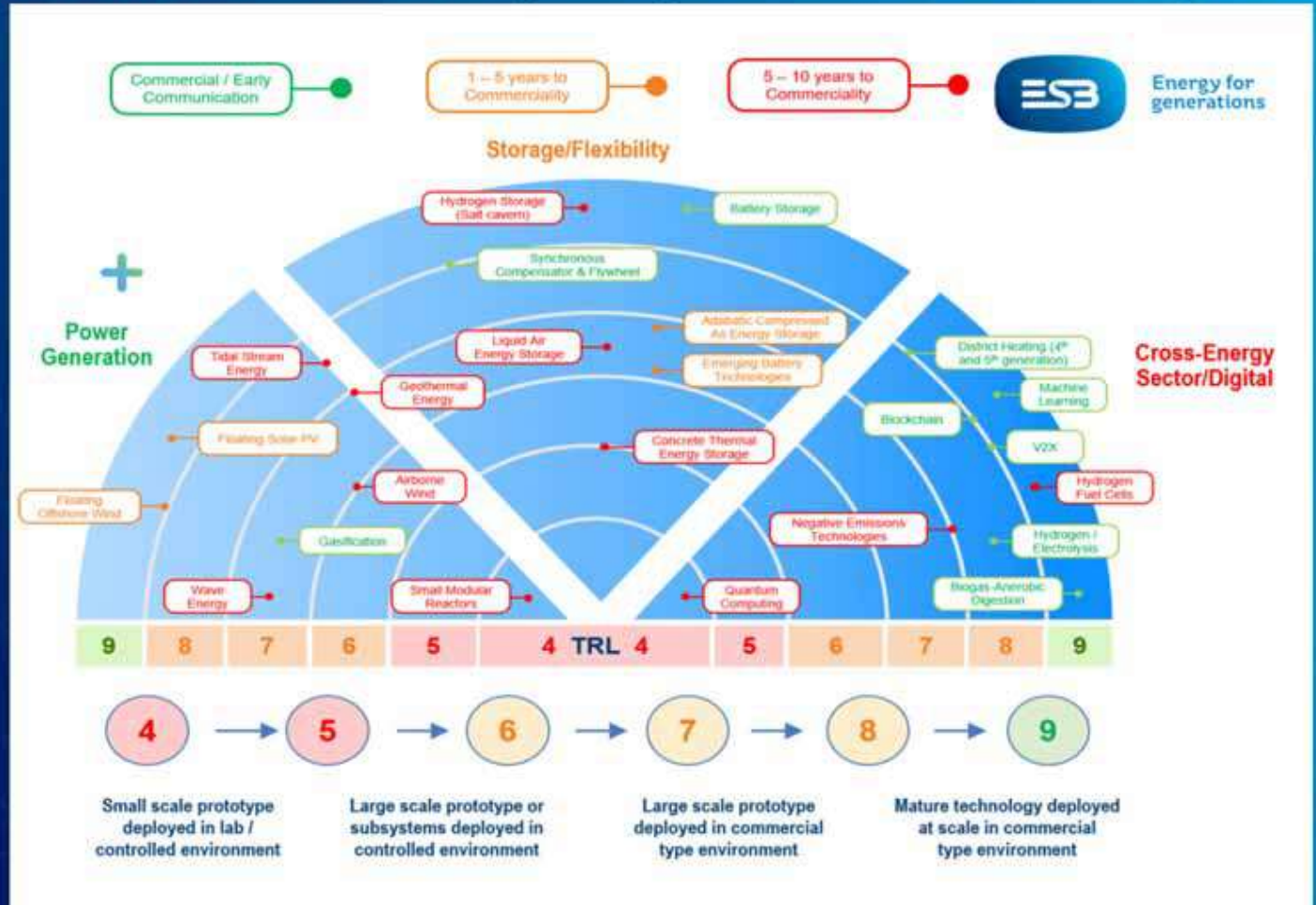
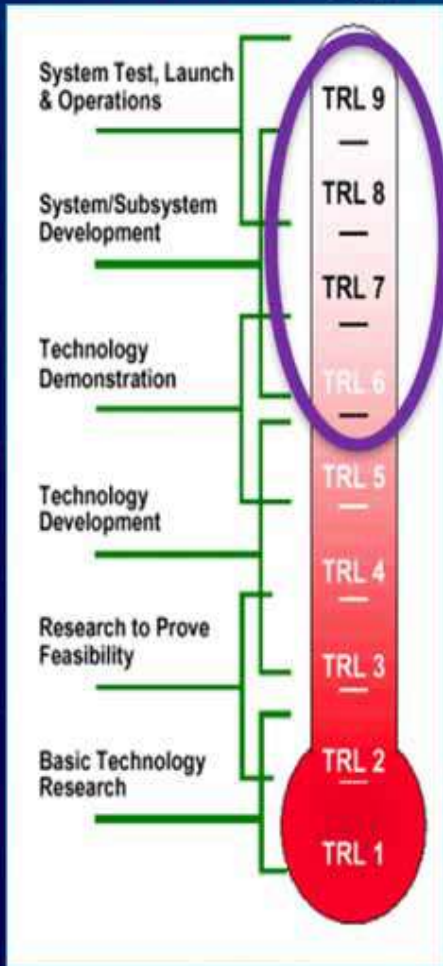


Overview of Innovation Strategy

- BU Innovation Projects
- Free Electrons
- Innovation Academy
- X-Potential
- Emerging Tech & R+D
- Innovation Recognition
- X-Site



Technology Readiness Levels (TRL) & Commerciality



Power Generation



Storage & Flexibility Technologies



Grid Scale Batteries TRL9



Flywheel + Synch-comp TRL9



Emerging battery technologies TRL7



Liquid Air Storage TRL 7



Concrete Storage TRL5-6



Hydrogen Storage TRL9



A-CAES TRL7

Cross Energy Sector Technologies



Industrial Heat Pumps TRL7



Vehicle to X TRL8-9



Negative Emissions TRL7-8



Biogas / AD TRL7-9



Hydrogen / Fuel Cells TRL7-9



Hydrogen / Electrolysis TRL6-9

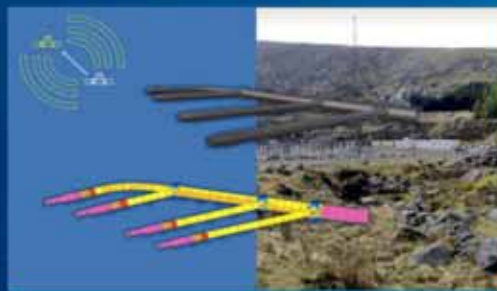


District Heating (4G & 5G) TRL 8-9

Digital Technologies



Blockchain TRL8-9



Machine Learning TRL9



Quantum Computing TRL 4

- Further increase of renewable energy generated from Wind Turbine Generators is challenging
- Resilience of older generators to more dynamic grid events is challenging
- Introduction of new technologies is necessary but challenging
- The introduction of the largest flywheel in the world is challenging
- New market is challenging
- Empowering the work force is challenging

John F. Kennedy: “We choose to go to the Moon, we choose to go to the Moon in this decade and do the other things, not because they are easy, but because they are hard, because that goal will serve to organize and measure the best of our energies and skills, because that challenge is one that we are willing to accept, one we are unwilling to postpone, and one which we intend to win, and the others, too.”